Sensitivity Analysis for Chaotic, Turbulent Flows

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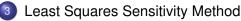
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Outline

Motivation



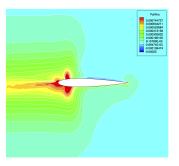
- Chaotic Sensitivity Analysis Issues
- Overview
- Kuramoto-Shivashinsky Equation
- NACA 0012



- Overview
- Multigrid Elimination



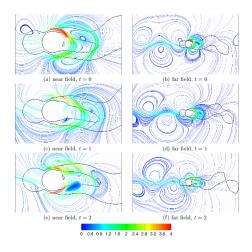
Sensitivity Anaylsis



- Sensitivity Analysis Methods compute derivatives of outputs with respect to inputs.
- With the adjoint, we go backwards in time to find the sensitivity of outputs to inputs.
- The computational cost of the Adjoint method DOES NOT scale with the number of gradients computed.

Adjoint Flow-Field

Sensitivities propagate upstream



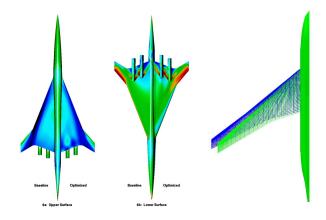
From Wang and Gao, 2012

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Sensitivity Analysis Applications

Aerodynamic Shape Optimization



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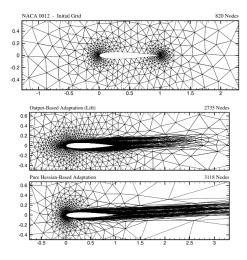
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From Jameson 2004

Sensitivity Analysis Applications

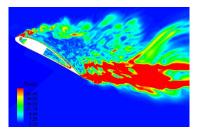
Error Estimation and Mesh Adaptation



From Venditti and Darmofal, 2003

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Sensitivity Analysis Applications Other Applications



From University of Miami CCS

- Flow Control
- Uncertainty Quantification
- and many more...

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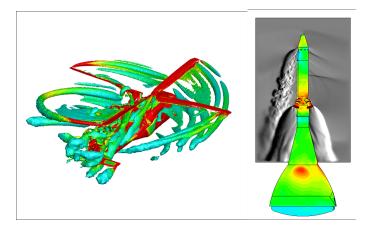
High Fidelity Model Issue



From DOE

- As computers become more powerful, high fidelity turbulence models such as LES will become increasingly popular.
- High fidelity models capture the chaotic nature of turbulent flows.
- However, traditional sensitivity analysis methods break down when applied to chaotic fluid flows.

Chaotic, Turbulent Flow-fields Unsteady Wakes

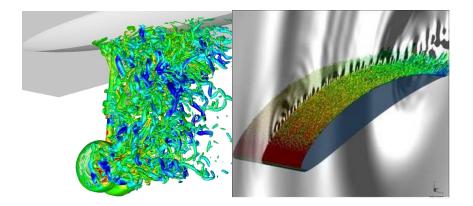


From E. Nielsen

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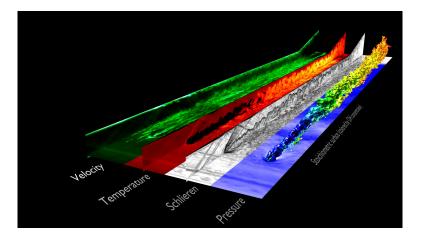
Chaotic, Turbulent Flow-fields Aeroaccoutics



LEFT: From E. Nielsen RIGHT: From TU Berlin



Chaotic, Turbulent Flow-fields Mixing



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From J. Larsson, Stanford University

Overview

Traditional Forward Sensitivity Analysis

 Interested in the long time averaged quantity J, governed by a system of equations f with some design parameter(s) s:

$$\bar{J} = \int_0^T J(u, s) dt, \quad \frac{\partial u}{\partial t} = f(u, s)$$

• Solve the tangent equation for $v = \frac{\partial u}{\partial s}$:

$$\frac{\partial \mathbf{v}}{\partial t} = \frac{\partial f}{\partial u}\mathbf{v} + \frac{\partial f}{\partial s}$$

• Compute the sensitivity of \overline{J} to s:

$$\frac{d\bar{J}^{T}}{ds} = \int_{0}^{T} \frac{\partial J}{\partial u} v + \frac{\partial J}{\partial s} dt$$

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Overview

Main Issue

• For chaotic systems, this does not work, because:

$$rac{dar{J}^{\infty}}{ds}
eq \lim_{T
ightarrow\infty}rac{dar{J}^{T}}{ds}$$

- This is because the tangent solution *v* diverges for chaotic systems. Counter-intuitively, increasing *T* can exacerbate this divergence.
- Adjoint sensitivity analysis breaks down for a similar reason.
- This property of chaotic systems has been shown by Lea et al. for the Lorenz Attractor.

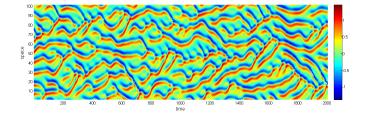
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• This problem exists for chaotic PDEs as well.

Chaotic KS Equation Solution



$$\frac{\partial u}{\partial t} = -u\frac{\partial u}{\partial x} - \frac{1}{R}\frac{\partial^2 u}{\partial x^2} - \frac{\partial^4 u}{\partial x^4}$$

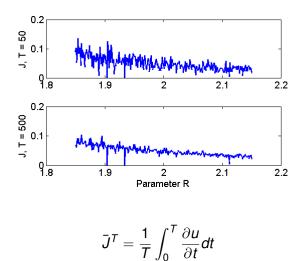
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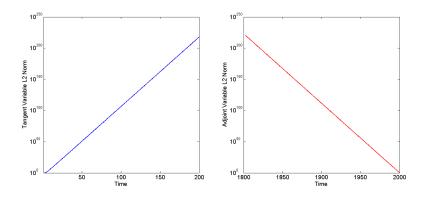
• R = 2.0 for Chaos in space and time.

Objective Function





Tangent and Adjoint Solutions



 Both Tangent and Adjoint solutions diverge exponentially for the KS equation.

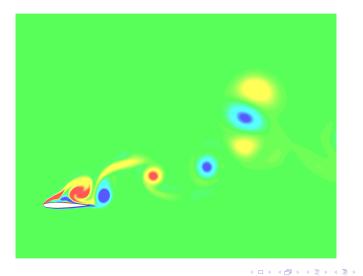
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Chaotic Sensitivity Analysis Issues NA

NACA 0012

NACA 0012 Airfoil Vorticity Contours Mach 0.1, Angle of Attack 20°, *Re* = 10000

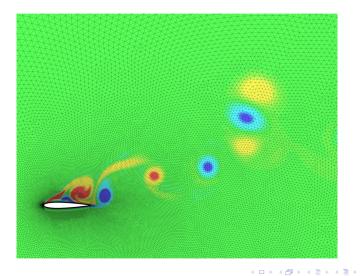




Chaotic Sensitivity Analysis Issues NA

NACA 0012

NACA 0012 Airfoil Vorticity Contours Mach 0.1, Angle of Attack 20°, *Re* = 10000

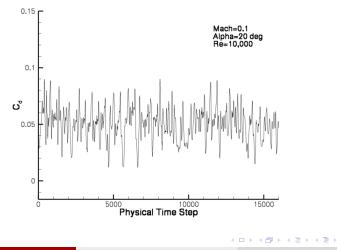




NACA 0012

Drag Coefficient Time History

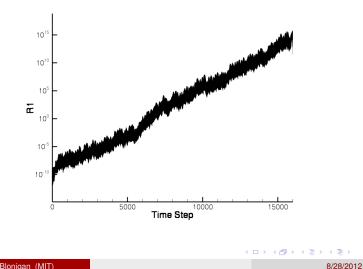
Aperiodicity indicates that the flow is chaotic



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Adjoint Residual L2 Norm



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Least Squares Sensitivity Method: The Basics

- A chaotic system has at least three different modes.
 - An unstable mode, associated with a positive Lyapunov Exponent.
 - A stable mode, associated with a negative Lyapunov Exponent.
 - A neutrally stable mode, associated with a zero Lyapunov Exponent.
- The unstable mode is responsible for the divergence of the tangent and adjoint equations.

Least Squares Sensitivity Method: The Basics (cont'd)

- Solve for stable modes forwards in time and solve unstable modes backward in time to prevent divergence of tangent and adjoint solutions.
- This solution is called the "Shadow Trajectory" (Wang, 2012) and is the least divergent tangent solution.
- Find the shadow trajectory by solving the following linearly contrained, least squares problem:

$$\min_{\eta, \mathbf{v}(t), 0 < t < T} \| \mathbf{v} \|_{2}, \quad \mathbf{s}.t. \quad \frac{\partial \mathbf{v}}{\partial t} = \frac{\partial f}{\partial u} \mathbf{v} + \frac{\partial f}{\partial d} + \eta f, \quad 0 < t < T$$

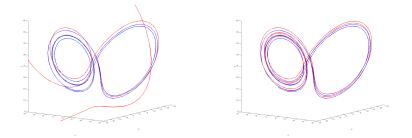
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Shadow Trajectory



• Divergent and Shadow trajectories for the Lorenz Attractor.



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LSS as a "Black Box"

$$\bar{J} = \int_0^T J(u, s) dt, \quad \frac{\partial u}{\partial t} = f(u, s)$$

Inputs:

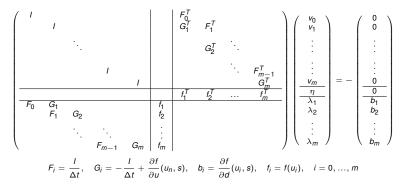
- Forward Solution: *u_i*
- Design Variable(s): s
- Operator values f_i
- Operator design parameter sensitivity $\frac{\partial f}{\partial s_i}$
- Objective Function Sensitivity: $\frac{\partial J}{\partial u_i}$
- Objective Function Sensitivity: $\frac{\partial J}{\partial s_i}$
- Jacobian matricies: $\frac{\partial f_i}{\partial u_i}$

Ouputs:

• Sensitivities: $\frac{d\bar{J}}{ds}$

Overview

KKT System



The KKT matrix is a large, symmetric block matrix, where each block is *n* by *n* for an *n* state system. Total size is 2mn + n + 1 by 2mn + n + 1 for *m* time steps. For a discretization with a five element stencil, there are approximately 23mn non-zero elements in the matrix.

• For the Airfoil simulation shown earlier the KKT matrix would be 3.2×10^9 by 3.2×10^9 with 3.7×10^{10} non-zero elements.



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Multigrid Elimination

- New method to reduce memory usage when solving the LSS KKT system.
- Gaussian Elimination conducted like 1D Multigrid.
- Eliminate every 2nd equation, reduce the system from 2mn + n + 1 to n + 1 equations.
- No need to save coefficients on every grid.
- Potentially Parallelizable.
- Method can be used to solve any unsteady system and its adjoint simultaneously.

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Schur Complement

- The KKT matrix is symmetric indefinite, so it becomes singular on coarser grids due to poor scaling.
- Instead, conduct ME on the KKT system's Schur Complement, which is SPD (ignoring the constraint equation).
- Original System:

$$\begin{bmatrix} I & B^T \\ B & 0 \end{bmatrix} \begin{bmatrix} v \\ \lambda \end{bmatrix} = -\begin{bmatrix} 0 \\ b \end{bmatrix}$$

Schur Complement:

 $BB^T \lambda = b$

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Multigrid Elimination

Elimination Scheme

Fine Grid Equations

$$L_{i-1}\lambda_{i-2} + D_{i-1}\lambda_{i-1} + U_{i-1}\lambda_i + f_{i-1}\eta = b_{i-1}$$
(1)
$$L_i\lambda_{i-1} + D_i\lambda_i + U_i\lambda_{i+1} + f_i\eta = b_i$$
(2)

$$L_{i+1}\lambda_i + D_{i+1}\lambda_{i+1} + U_{i+1}\lambda_{i+2} + f_{i+1}\eta = b_{i+1}$$
(3)



Elimination Scheme Coarse Grid Equation

$$L_{I}\lambda_{i-2} + D_{I}\lambda_{i} + U_{I}\lambda_{i+2} + f_{I}\eta = b_{I}$$

Where:

$$\begin{array}{rcl} L_{l} = & -L_{i}D_{i-1}^{-1}L_{i-1} \\ D_{l} = & -L_{i}D_{i-1}^{-1}U_{i-1} + D_{i} - U_{i}D_{i+1}^{-1}L_{i+1} \\ U_{l} = & -U_{i}D_{i+1}^{-1}U_{i+1} \\ f_{l} = & -L_{i}D_{i-1}^{-1}f_{i-1} + f_{i} - U_{i}D_{i+1}^{-1}f_{i+1} \\ b_{l} = & -L_{i}D_{i-1}^{-1}b_{i-1} + b_{i} - U_{i}D_{i+1}^{-1}b_{i+1} \end{array}$$

• A similar method is used to restrict the constraint equation and the equation for the long-time averaged gradient of interest.

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LSS and ME applied to the Lorenz Equations

Lorenz Equations:

$$\frac{dx}{dt} = s(y-x), \quad \frac{dy}{dt} = x(r-z) - y, \quad \frac{dz}{dt} = xy - bz$$

Long time averaged z gradients computed by LSS/ME:

$$rac{dar{z}}{ds} = 0.1545, \quad rac{dar{z}}{dr} = 0.9709, \quad rac{dar{z}}{db} = -1.8014$$

• Gradients computed by finite difference/linear regression:

$$rac{dar{z}}{ds} = 0.16 \pm 0.02, \quad rac{dar{z}}{dr} = 1.01 \pm 0.04, \quad rac{dar{z}}{db} = -1.68 \pm 0.15$$

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Avoiding inverting Matrices

- ME can be implemented so that no Jacobian matrices need to be inverted
- Consider the following system:

$$\left(\begin{array}{ccc} D_1 & U_1 & 0\\ L_2 & D_2 & U_2\\ 0 & L_3 & D_3 \end{array}\right) \left(\begin{array}{c} \lambda_1\\ \lambda_2\\ \lambda_3 \end{array}\right) = \left(\begin{array}{c} b_1\\ b_2\\ b_3 \end{array}\right)$$

• The system is restricted using ME:

$$A\lambda_2 = b$$

with:

$$\begin{array}{ll} A = & -L_2 D_1^{-1} U_1 + D_2 - U_2 D_3^{-1} L_3 \\ b = & -L_2 D_1^{-1} b_1 + b_2 - U_2 D_3^{-1} b_3 \end{array}$$



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Avoiding inverting Matrices (cont'd)

 This system can be solved iteratively, using some preconditioner P:

$$P\Delta x = b - Ax_k, \quad x_{k+1} = x_k + \Delta x$$

Where x_k is the value of λ_2 after *k* iterations.

• Decompose Ax_k into three parts:

$$Ax_{k} = -L_{2}D_{1}^{-1}U_{1}x_{k} + D_{2}x_{k} - U_{2}D_{3}^{-1}L_{3}x_{k} = \alpha + \beta + \gamma$$



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Avoiding inverting Matrices (cont'd)

• Consider α :

$$-L_2 D_1^{-1} U_1 x_k = \alpha$$

• Compute
$$y_k = U_1 x_k$$
:
 $-L_2 D_1^{-1} y_k = \alpha$

• Next, define $z_k = D_1^{-1} y_k$. Itertively solve:

$$D_1 z_k = y_k$$

• Use the result to compute α :

$$\alpha = -L_2 z_k$$

 This idea can be applied to a much larger system and allows ME to be conducted without inverting any Jacobian matricies.

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Conclusion

- Traditional sensitivity analysis methods are unable to compute sensitivities of long-time averaged quantities in CFD simulations.
- The LSS method could compute these quantities in an efficient manner if applied with Multigrid elimination.
- Future Work
 - Further develop and implement ME without inverting Jacobians, ideally in C, C++ or Fortran.
 - Apply LSS/ME to the KS equation.
 - Validate LSS on aerodynamic test cases.

Acknowledgements



I would like the acknowledge the following people for their guidance and support this summer:

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- Johan Larsson
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