

Session 13: Thermochemical Nonequilibrium Simulations

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Session Overview

- Background
- Restrictions (ITAR)
- New Required Data Files
- Set-up fun3d.nml
- New Boundary Conditions
- Required Command Line Option
- Challenges to Stagnation Region Heating
 - Multi-dimensional Reconstruction
- Examples
- Future Plans



Code Background

LAURA (1987 - present)

Langley Aerothermodynamic Upwind Relaxation Algorithm

Multi-block, structured grid, cell-centered, finite-volume

Thermochemical equilibrium and nonequilibrium (Earth, Mars) with Park's two-temperature model

Roe's scheme, Yee's STVD limiter, Harten's entropy fix, central difference viscous terms (the devil I know!)

Tuned for Cray vector architecture - extensive use of conditional compilation

FUN3D (perfect gas, 1989 - present)

Unstructured grid, node-based, finite volume

perfect gas, incompressible to supersonic domains

Multiple upwind options including Roe's scheme, weighted least-squares gradients into Barth or Venkat limiter, Green-Gauss viscous terms

Adjoint equation solution for grid adaptation and optimization



Merged Code

FUN3D (Generic Gas Path, 2001 - present)

- Re-factor FUN3D to accommodate multiple species, energies, momenta, coupled 2eq turbulence models

- Create PHYSICS MODULES directory to bring thermodynamic, kinetic, transport, and turbulence models from LAURA and VULCAN into FUN3D

- Adopt Extreme Programming conventions with continuous, automated testing

LAURA V (2005 - present)

- Production capability in FUN3D slow to mature

 - Poor quality heating on tetrahedral grids

 - Columbia accident investigation and Return to Flight

- Re-factored LAURA using FUN3D data structures and modules

 - PHYSICS MODULES

 - Continuous, automated code testing

- Modular structure simplified addition of HARA radiation and ablation



Restrictions

- ITAR - International Traffic in Arms Regulations
 - US Government codes explicitly written for simulation of flows over vehicles traveling at hypersonic velocities are treated as ITAR restricted
 - Contents of the PHYSICS_MODULES directory contain the models required for high temperature gas dynamic simulations
 - Baseline FUN3D contains only perfect gas models and is not considered ITAR (though it is export controlled)
 - Contents of PHYSICS_MODULES are treated as ITAR - are not released unless specifically requested and approved
- A separate request for the generic gas path and a new usage agreement are required



Configuration

Follow instructions for baseline FUN3D but include one additional option:

```
../configure --enable-hefss ...
```

(hefss: high energy flow solver synthesis)



PHYSICS_MODULES

- equilibrium_air.f90
- [hara_radiation.f90](#)
- shared_gas_variables.f90
- [shared_hara_variables.f90](#)
- catalysis.f90
- surface.f90
- chemical_kinetics.f90
- thermal_relaxation.f90
- thermodynamics.f90
- transport_property.f90
- [turb_gen.f90](#)

Data files - should not need modification

- kinetic_data
- species_thermo_data
- species_transp_data
- species_transp_data_0

Data file - modify to define thermochemical model

- [tdata](#)



Thermochemical nonequilibrium model: tdata

Two Temperature

Thermal nonequilibrium

N 6.217e-20

O 7.758e-09

N2 0.737795

O2 0.262205

NO 1.e-09

N+ 7.261e-35

O+ 1.179e-35

N2+ 1.495e-35

O2+ 3.785e-33

NO+ 4.567e-24

e- 8.352e-29

Species name followed by mass
fraction in mixture



Air as Perfect Gas in tdata

perfect_gas

DEFAULTS for air are:

$\gamma = 1.4$

$\text{mol_wt} = 28.8$

$\text{suther1} = 0.1458205\text{E-}05$

$\text{suther2} = 110.333333$

$\text{prand} = 0.72$



Generic Perfect Gas in tdata

perfect_gas

&species_properties

gamma =

Ratio of specific heats

mol_wt =

Molecular weight

suther1 =

Sutherland constant 1

suther2 =

Sutherland constant 2

prandl =

Prandtl number

/



Sutherlands Constants in tdata

Note that the constants for Sutherland's law in the namelist species_properties define viscosity in SI units using the equation:

$$\mu = suther1 \frac{T^{3/2}}{T + suther2}$$

Constants for Sutherland's law often appear in other units and/or in the form

$$\mu = \mu_{ref} \left(\frac{T}{T_{ref}} \right)^{3/2} \frac{T_{ref} + suther2}{T + suther2}$$

$$suther1 = \mu_{ref} \frac{T_{ref} + suther2}{T_{ref}^{3/2}}$$



Equilibrium Gas in tdata

equilibrium_air_t

tannehill model

equilibrium_air_r

eq_air_coeffs.asc

eq_air_lk_up.asc



Recommended Model for Return from LEO in tdata

N 0.

O 0.

N2 0.737795

O2 0.262205

NO 0.



Generic Gas Options in fun3d.nml

```
&governing_equations  
  eqn_type = "generic"  
  viscous_terms = "laminar"  
  chemical_kinetics = "finite-rate"  
  thermal_energy_model = "frozen"  
/
```

eqn_type: cal_perf_compress, cal_perf_incompress, **generic**
viscous_terms: **inviscid**, **laminar**, turbulent
chemical_kinetics: **frozen**, **finite-rate**
(only engaged if tdata contains two or more species names)
thermal_energy_model: **frozen**, **non-equilib**
(only engaged if first line of tdata is "two temperature")



Generic Gas Options in fun3d.nml

```
&reference_physical_properties  
  gridlength_conversion = .0254  
  dim_input_type = "dimensional-SI"  
  temperature_units = "Kelvin"  
  velocity = 6920.0  
  density = 5.750E-005  
  temperature = 202.0  
  temperature_walldefault = 800.0  
  angle_of_attack = -50.6  
  angle_of_yaw = 0.0
```

/

The generic gas path does not accept Mach number and Reynolds number to define free stream conditions.



Generic Gas Options in fun3d.nml

```
&inviscid_flux_method  
  flux_limiter = "minmod"  
  first_order_iterations = 0  
  flux_construction = "stvd"  
  multi_dim_recon_flag = 0 (0,1,2)  
  re_cell_cutoff = 400.0000 (NA)  
  re_cell_cutoff_expon = 8 (NA)  
  re_cell_cutoff_dir = 2 (freq. update direction)  
  rhs_u_eigenvalue_coef = 0.5  
  lhs_u_eigenvalue_coef = 1.0
```

/



Generic Gas Options in fun3d.nml

&nonlinear_solver_parameters

time_accuracy = "steady" steady, 1st order

time_step_nondim = 1.0

pseudo_time_stepping = "on"

subiterations = 2

schedule_number = 2

schedule_iteration = 1 200

schedule_cfl = 5.e+06 5.e+06

invis_relax_factor = 2.

visc_relax_factor = 1.



Generic Gas Options in fun3d.nml

```
&linear_solver_parameters
```

```
  meanflow_sweeps = 2
```

```
  line_implicit = "off"
```

```
/
```

meanflow_sweeps: 1 or 2 to initialize, 20 to 30
final



Generic Gas Options in fun3d.nml

```
&code_run_control  
  steps = 10000  
  stopping_tolerance = 1.00E-100  
  restart_write_freq = 500  
  restart_read = "on"  
  jacobian_eval_freq = 1  
/
```

jacobian_eval_freq: keep small until shock sets up
convergence is judged by heating - expect residual to freeze

(Note that the command line option `--no_smart_jupdate` must be invoked in order that the `jacobian_eval_freq` is engaged.)



Additional Surface Boundary Conditions

4001 - 4009: map from 1st to 9th occurrence of namelist
&surface_properties in file surface_property_data

```
&surface_properties
```

```
surface_group_name = "RCG"
```

```
surface_temperature_type = "radiative equilibrium"
```

```
emiss_a = 0.89
```

```
catalysis_model = "Stewart-RCG"
```

```
/
```



Additional Surface Boundary Conditions

surface_group_name: your identifying name

surface_temperature_type: **constant, adiabatic, radiative equilibrium,**
surface_energy_balance

$$\varepsilon = emiss_a + T(emiss_b + T(emiss_c + T(emiss_d)))$$

$$q = \varepsilon \sigma T^4$$

surface_temperature: specify value if **constant** different from default

catalysis_model: **super-catalytic, non-catalytic,** equilibrium-catalytic, **Stewart-RCG, Zoby-RCG, Scott-RCG, fully-catalytic**



Catalytic Boundary Conditions

Super-catalytic: Species mass fractions set to free stream conditions

Equilibrium-catalytic: Species mass fractions in equilibrium at wall temperature and pressure

Fully-catalytic: 100% of atoms diffusing to wall recombine to form homogeneous, neutral diatom. All other ions are neutralized.

Finite-catalytic: Fraction of atoms undergoing homogeneous recombination is function of wall temperature.

Non-catalytic: $J_i = 0$



Execution

For the near term the generic path requires use of command line option: **--Impi_io 0**

nodet_mpi --Impi_io 0

party --Impi_io 0

This path carries additional data for restart and post-processing and the requisite updates for Version 11 io have not been completed.



Goals

Start with “reasonable grid” on CAD
description of vehicle / system of arbitrary
complexity

“Reasonable” means sufficient resolution to
initialize a CFD simulation.

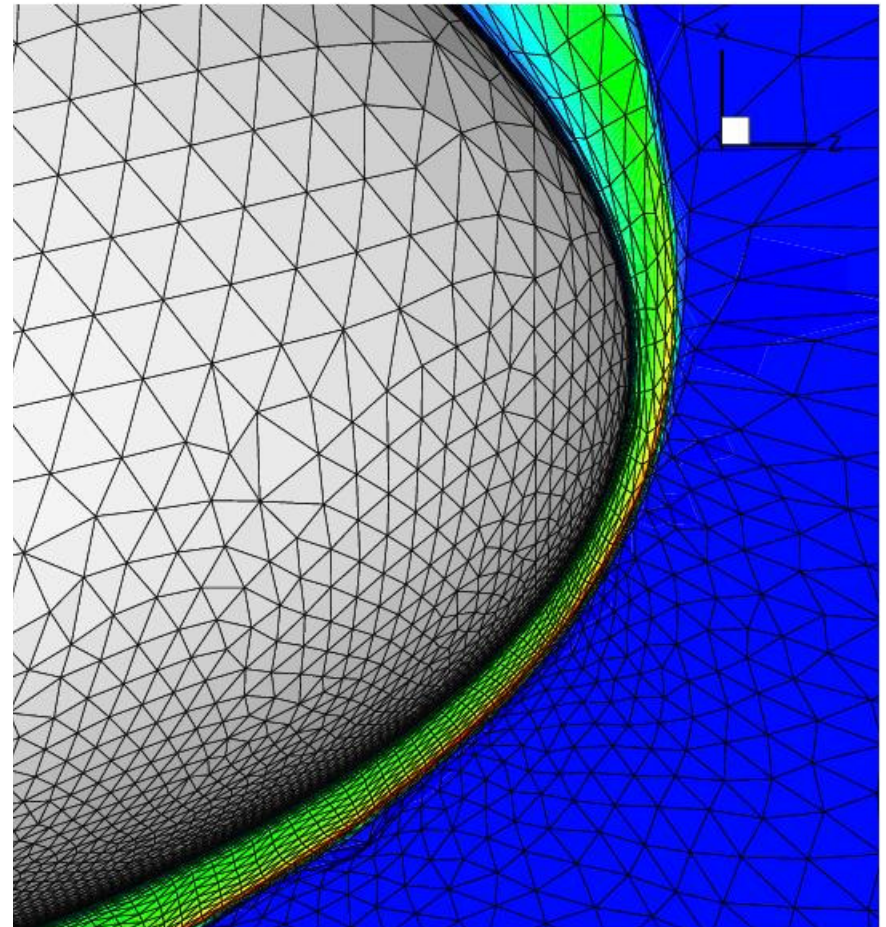
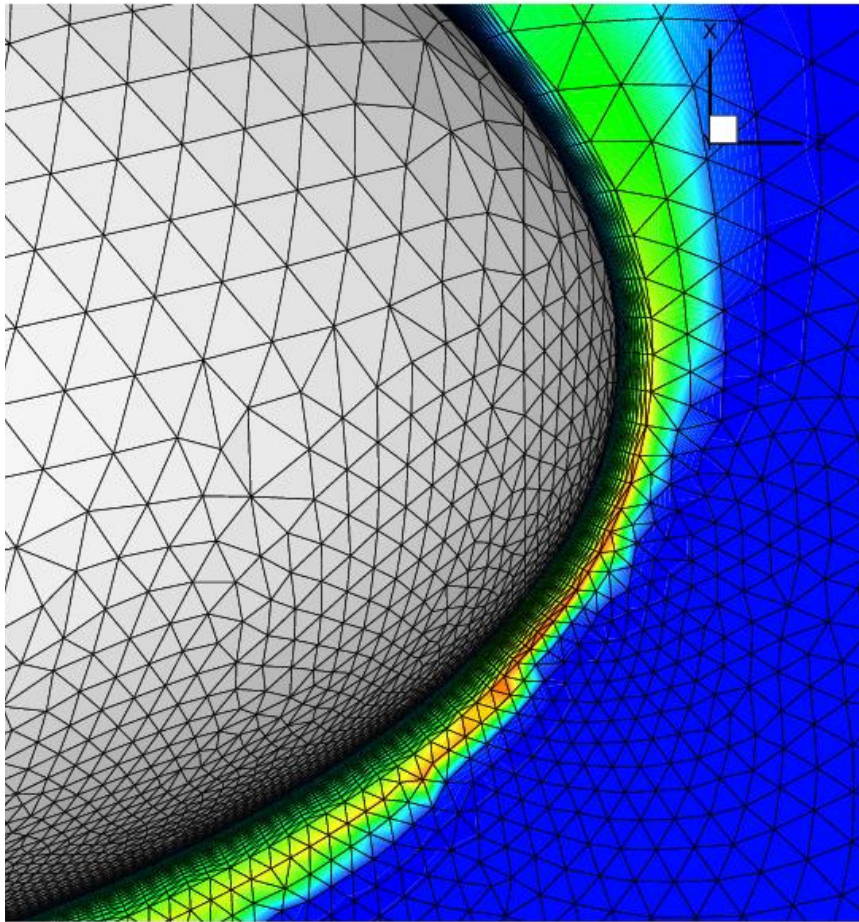
Finish with CFD simulation accurate to user
specified convergence criteria with physics
model uncertainties bounded by validation
tests.



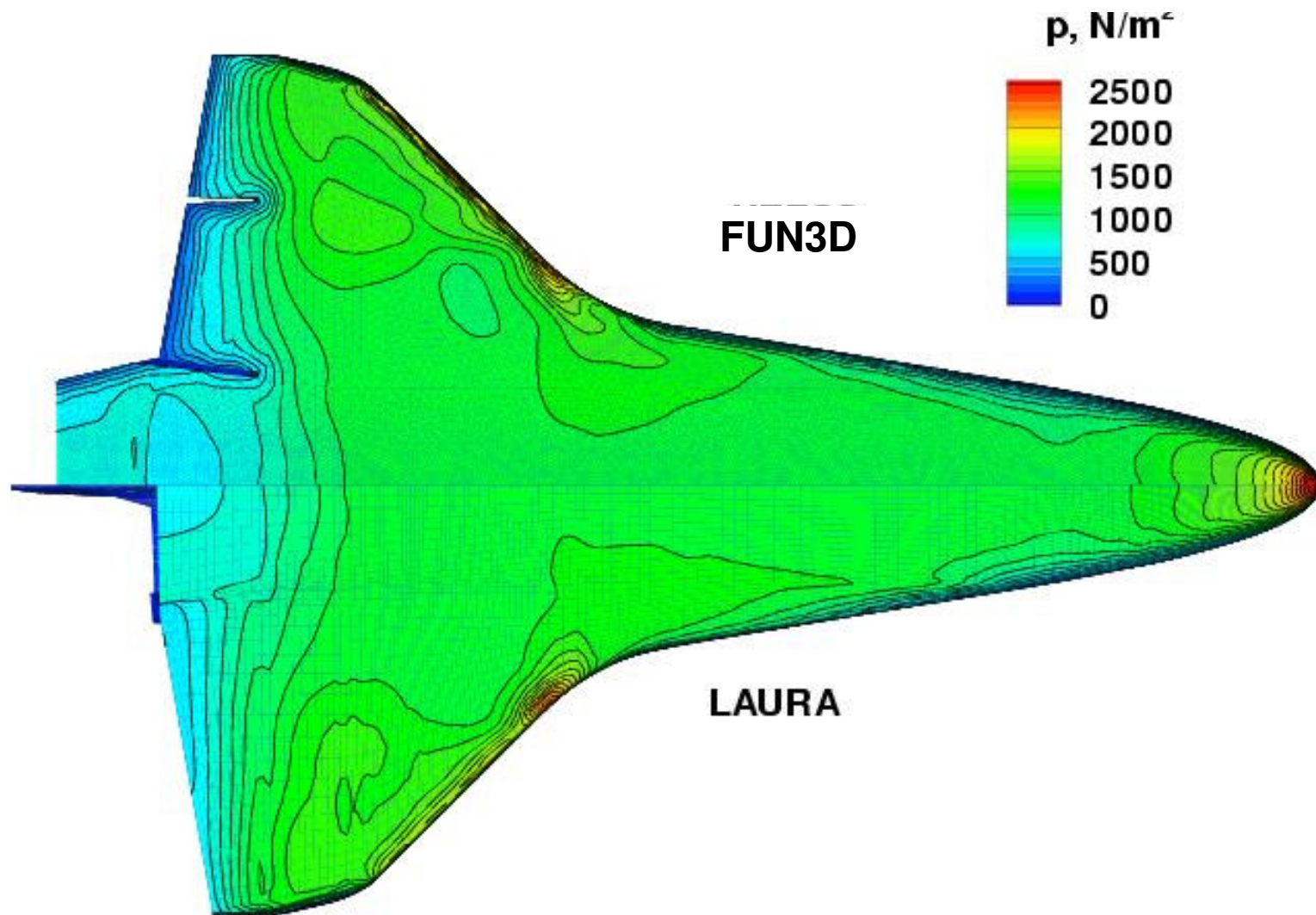
Shuttle Forebody Grids

STS-2 72.4 km

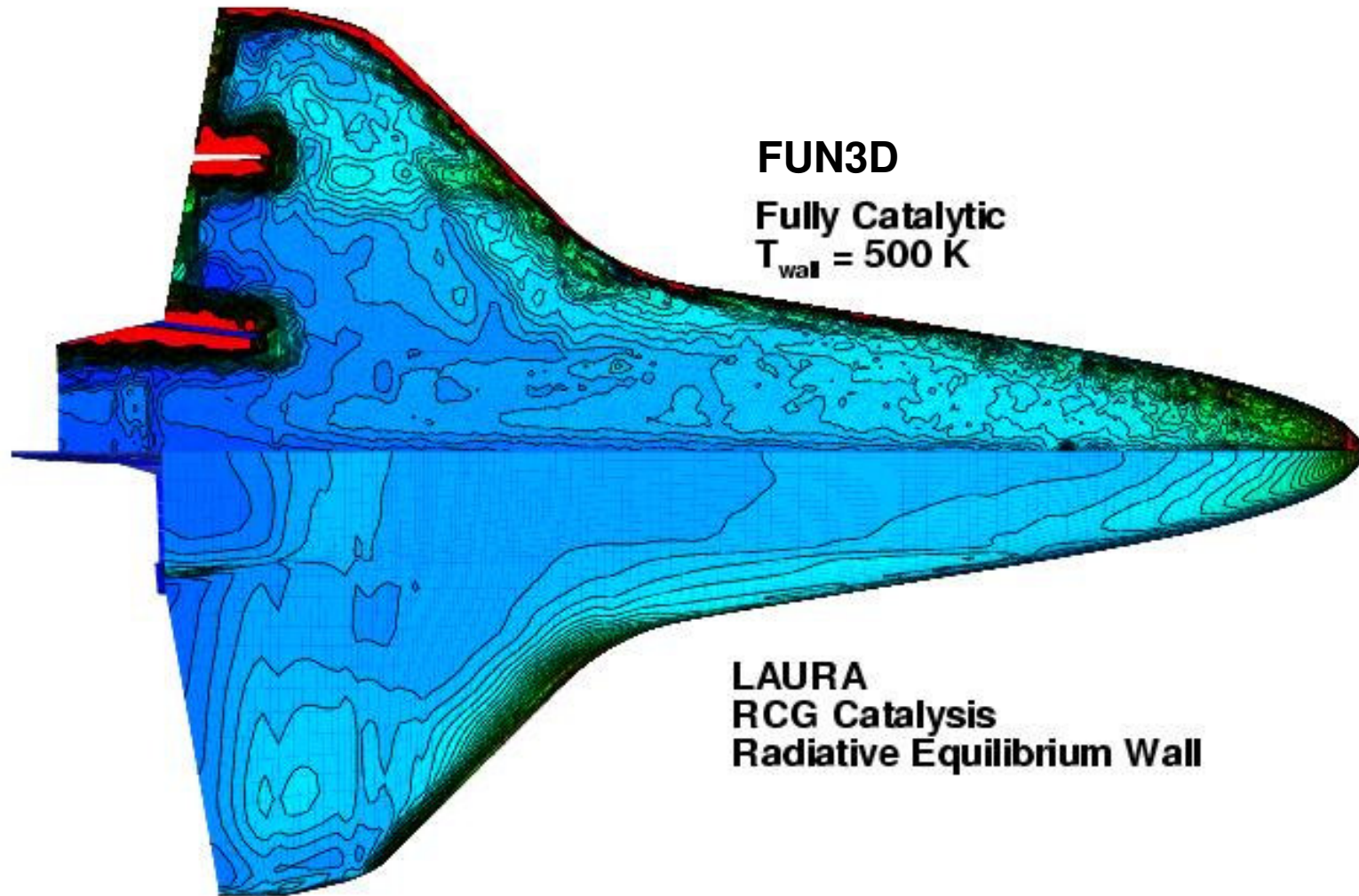
$V_\infty = 6920$ m/s $\rho_\infty = 5.75 \cdot 10^{-5}$ kg/m³ $\alpha = 39.4$ deg



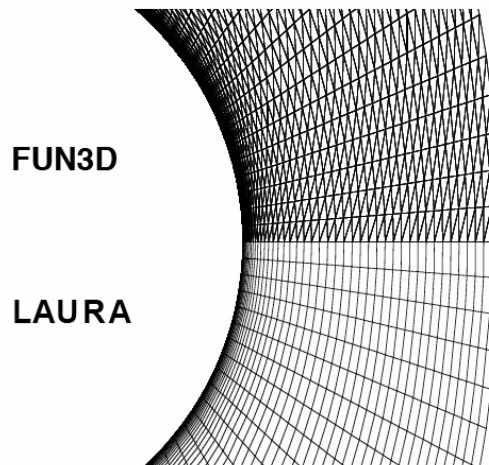
Windside Pressure Contours



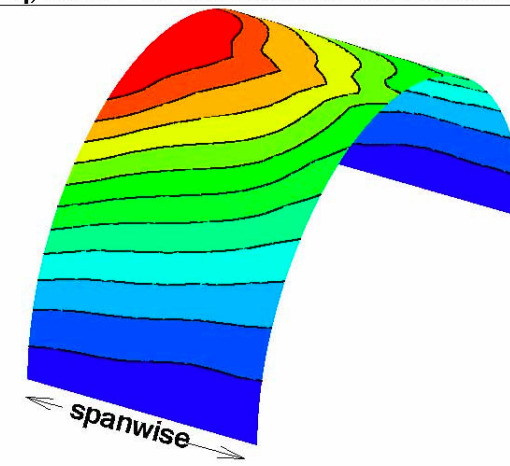
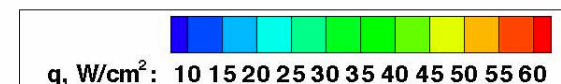
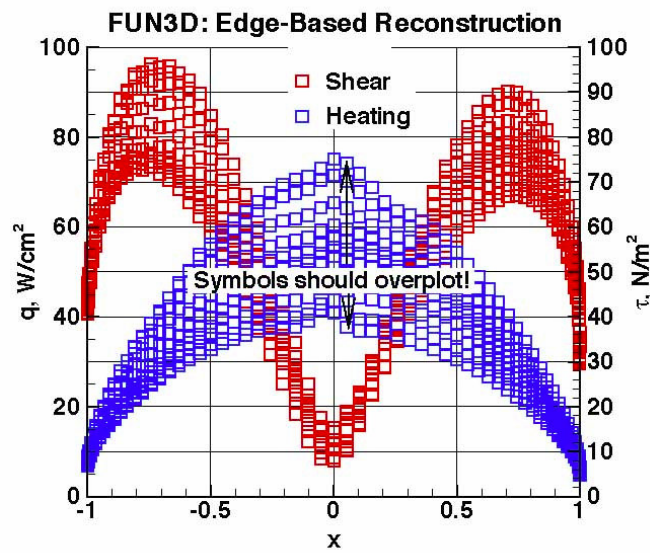
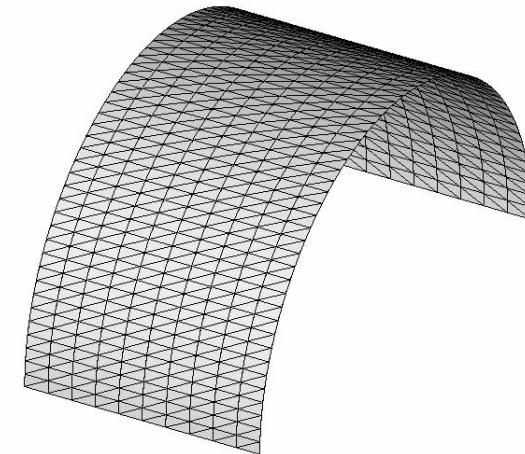
Windside Heating Contours



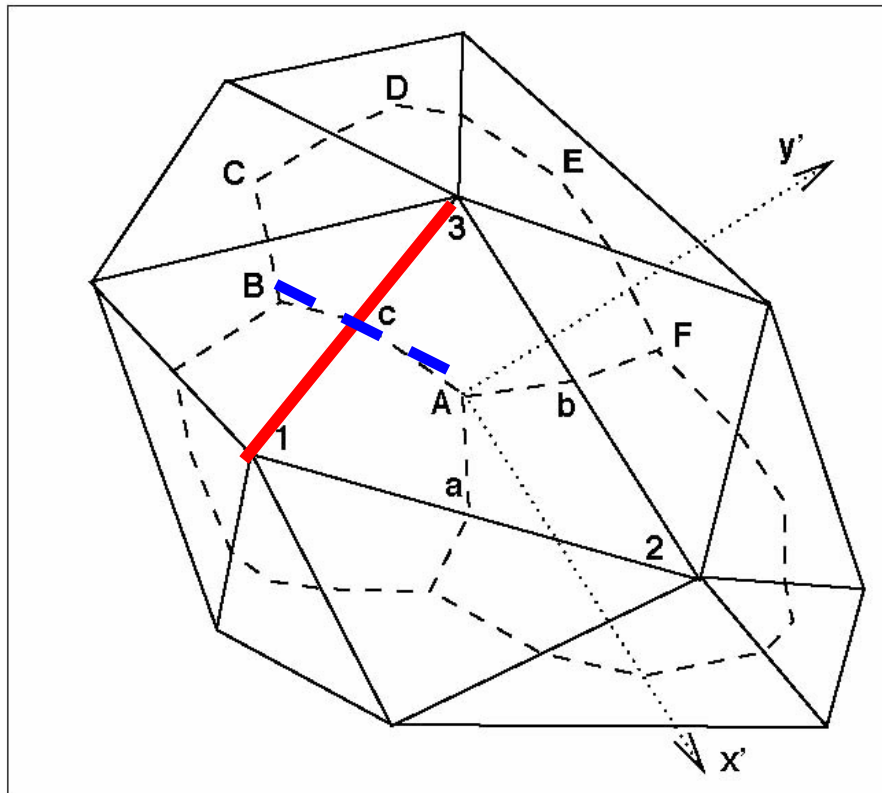
The Challenge Problem - Mach 17 Flow Over Cylinder



Surface Grid



One Dimensional, Edge Based Reconstruction

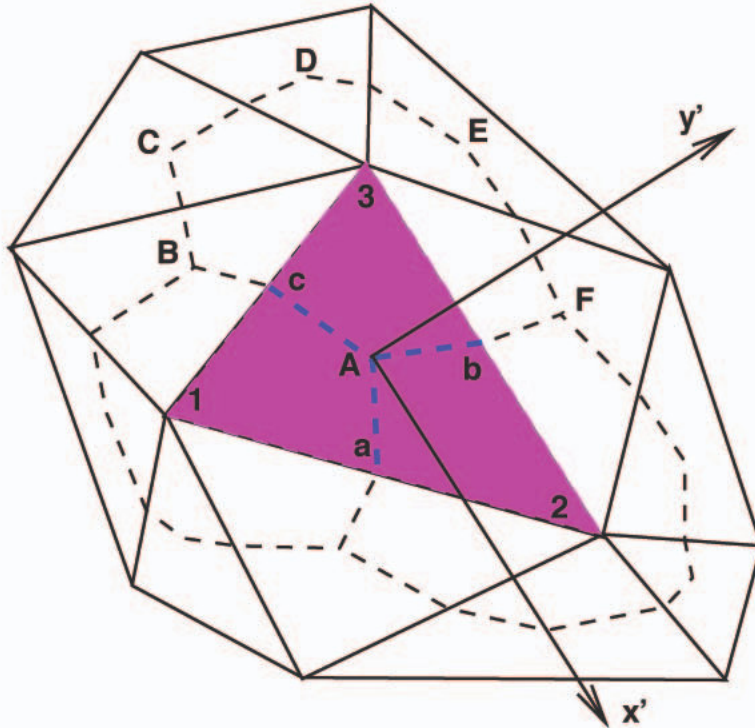


Loop over edges (red)

Compute flux f_c across single face separating two nodes (blue)

$$f_c(q_1, q_3, \nabla q_1, \nabla q_3)$$

Three-Dimensional, Element Based Reconstruction



The metrics used here are identical to those already used in the viscous flux formulation.

Loop over elements (magenta)

Compute flux f_{cAa} , f_{cAb} , and f_{bAa} for the three faces (blue) separating the three nodes defining the element

$$f_{cAa} = f_{x'} n_{cAa,x'} + f_{y'} n_{cAa,y'}$$

$$f_{cAb} = f_{x'} n_{cAb,x'} + f_{y'} n_{cAb,y'}$$

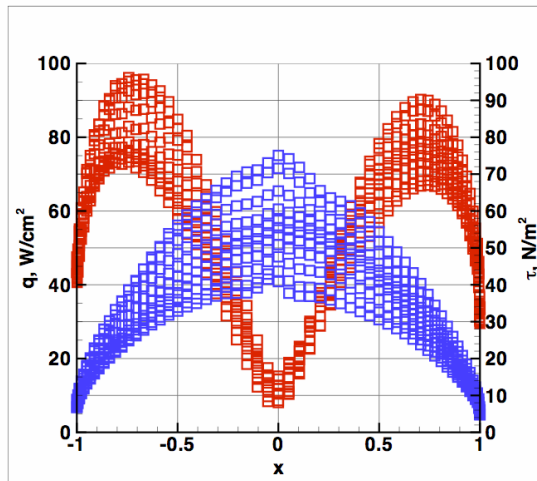
$$f_{bAa} = f_{x'} n_{bAa,x'} + f_{y'} n_{bAa,y'}$$

$$f_{x'}(q_{R,x'}, q_{L,x'}, \nabla q_{R,x'}, \nabla q_{L,x'})$$

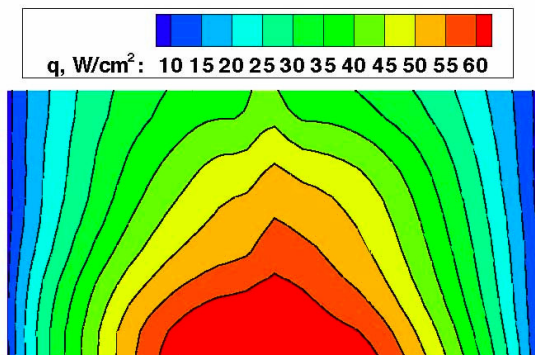
$$f_{y'}(q_{R,y'}, q_{L,y'}, \nabla q_{R,y'}, \nabla q_{L,y'})$$

Challenge Problem Revisited

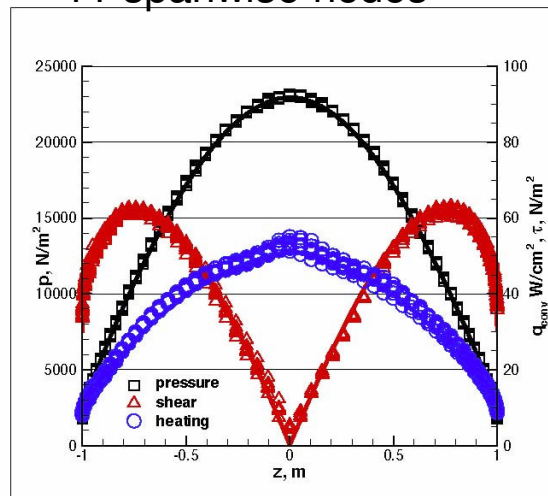
Original



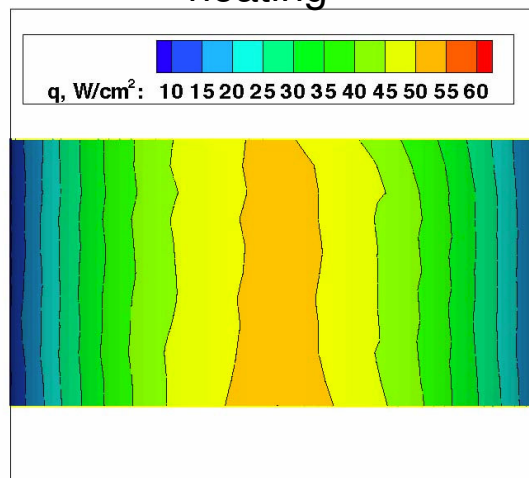
heating



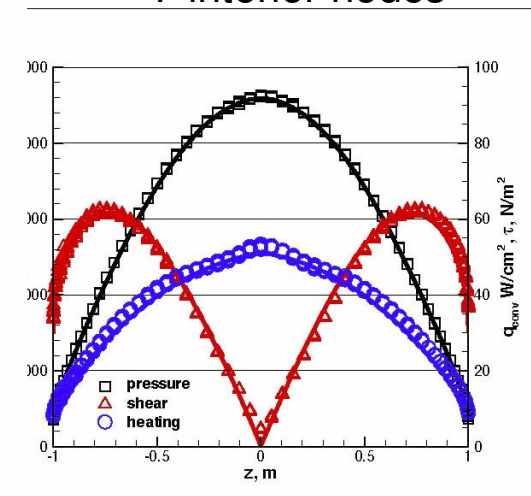
11 spanwise nodes



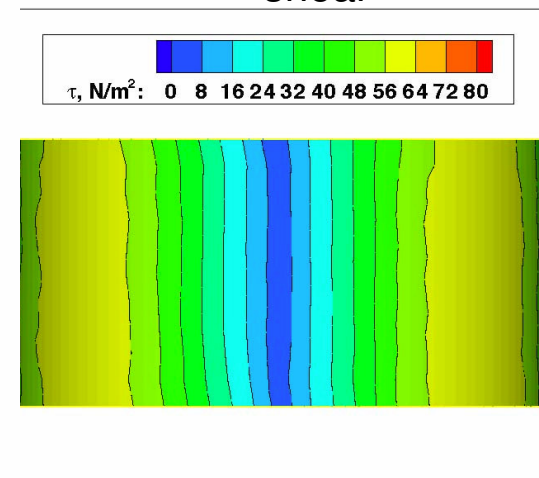
heating



7 interior nodes



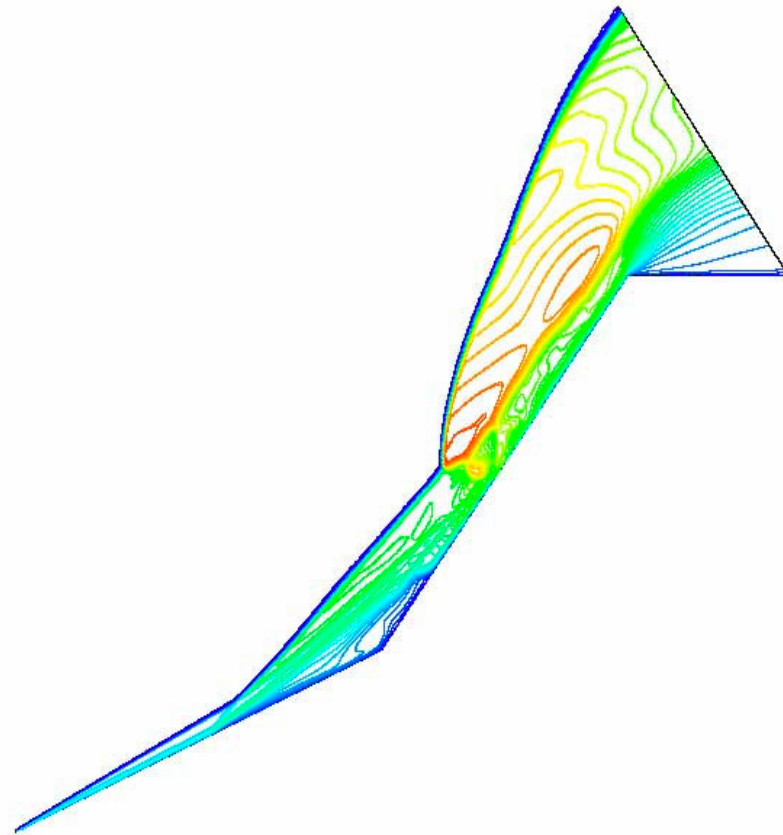
shear



Sharp Double-Cone

Temperature

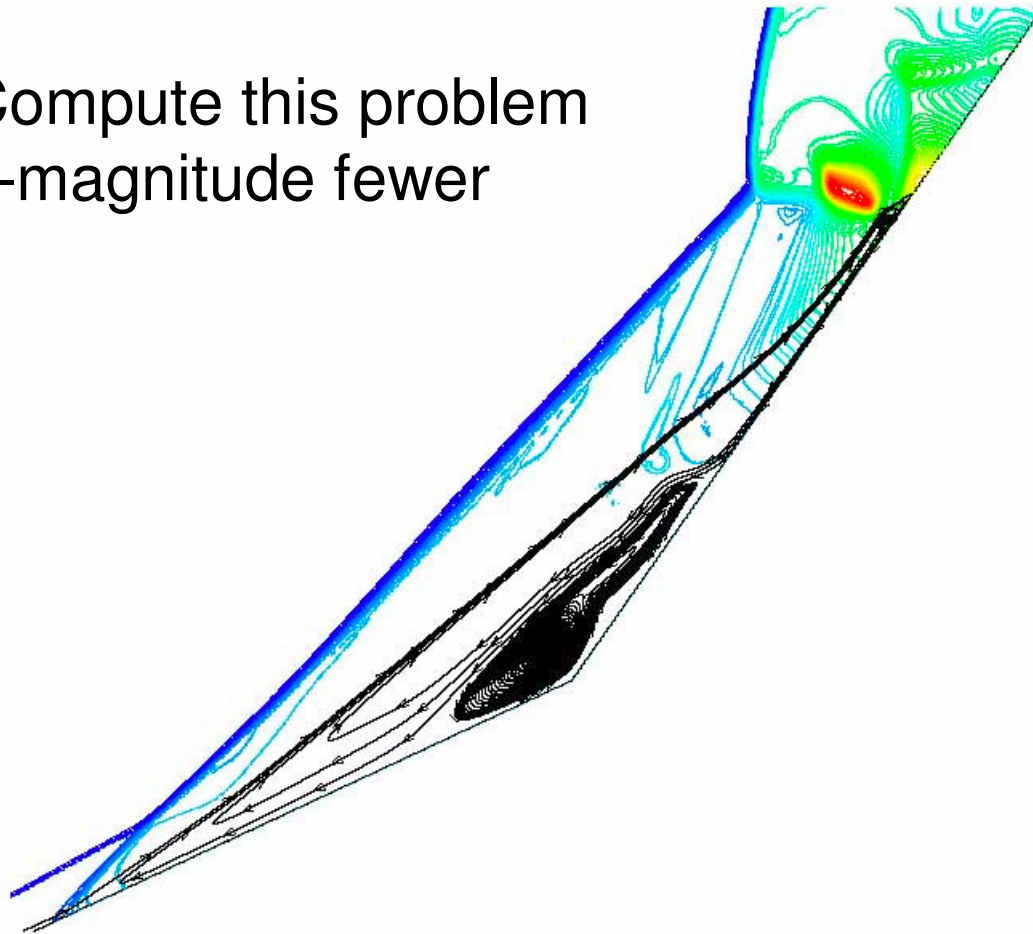
Run 28 (Holden et. al)
Mach 9.6
 $Re = 144000 \text{ m}^{-1}$
perfect gas (N_2)



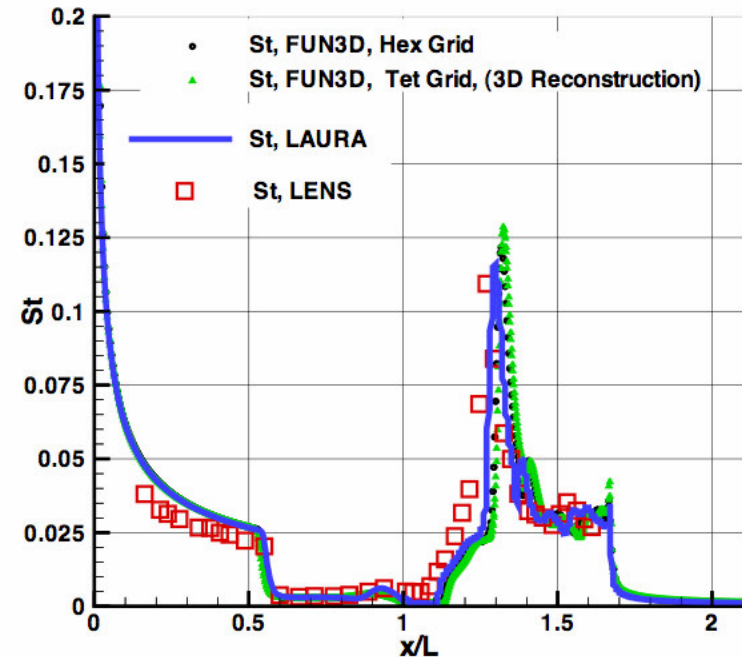
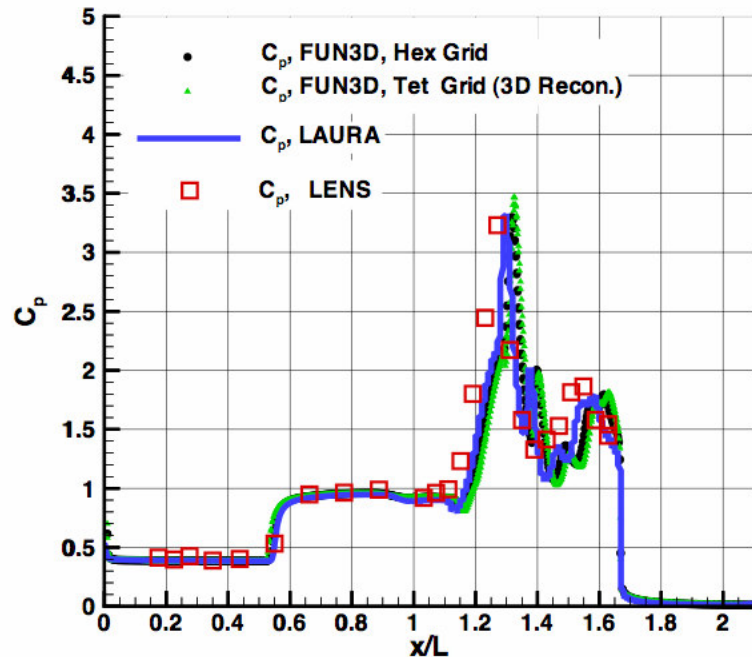
Sharp Double-Cone -- Separation Zones

Pressure

Challenge: Compute this problem with order-of-magnitude fewer mesh points.



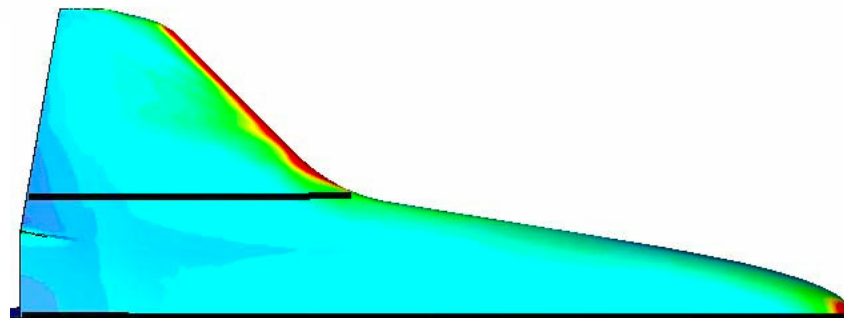
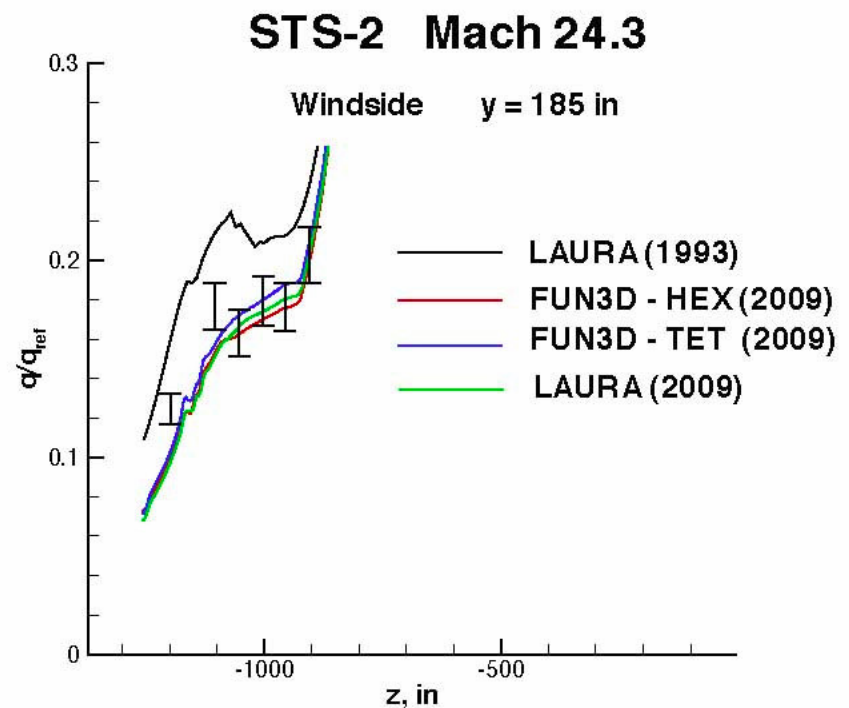
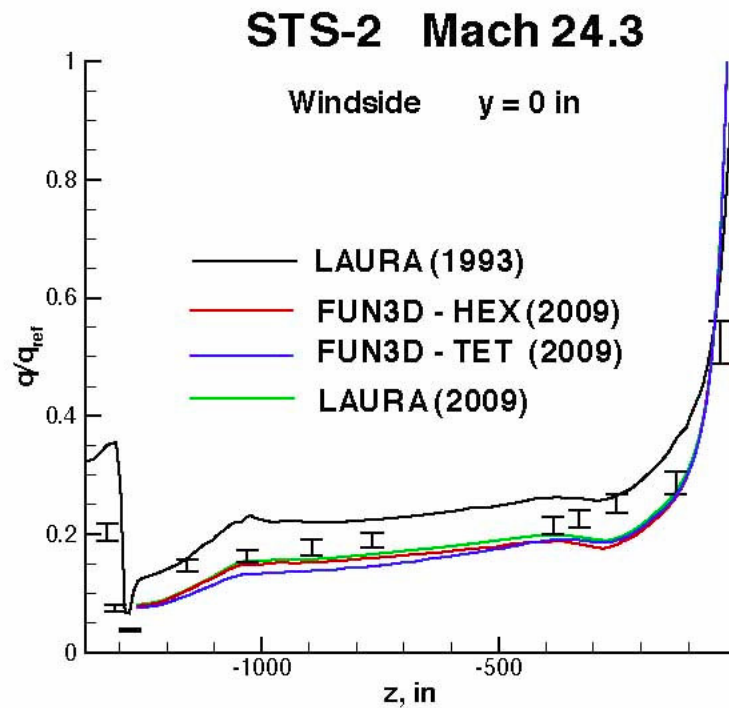
Sharp Double-Cone - Surface Pressure and Heating



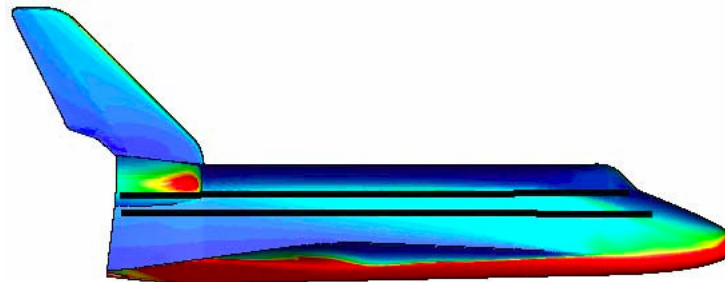
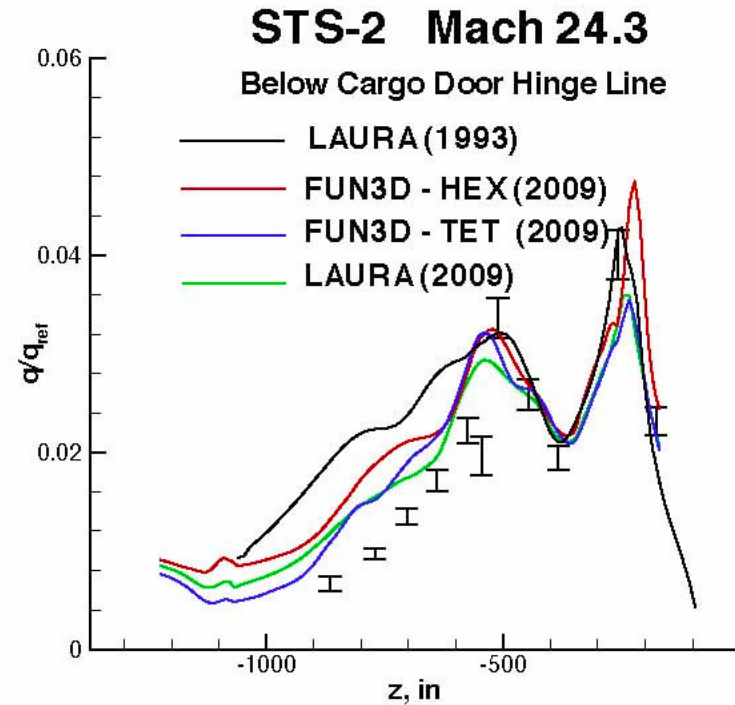
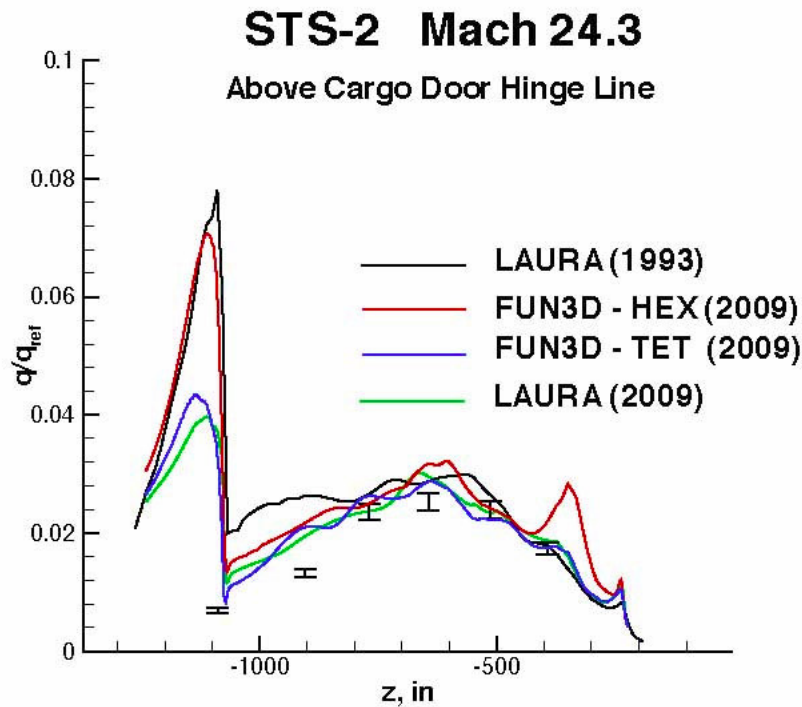
- Good agreement between codes and grid types.
- FUN3D multi-dimensional reconstruction had to be run time accurate.



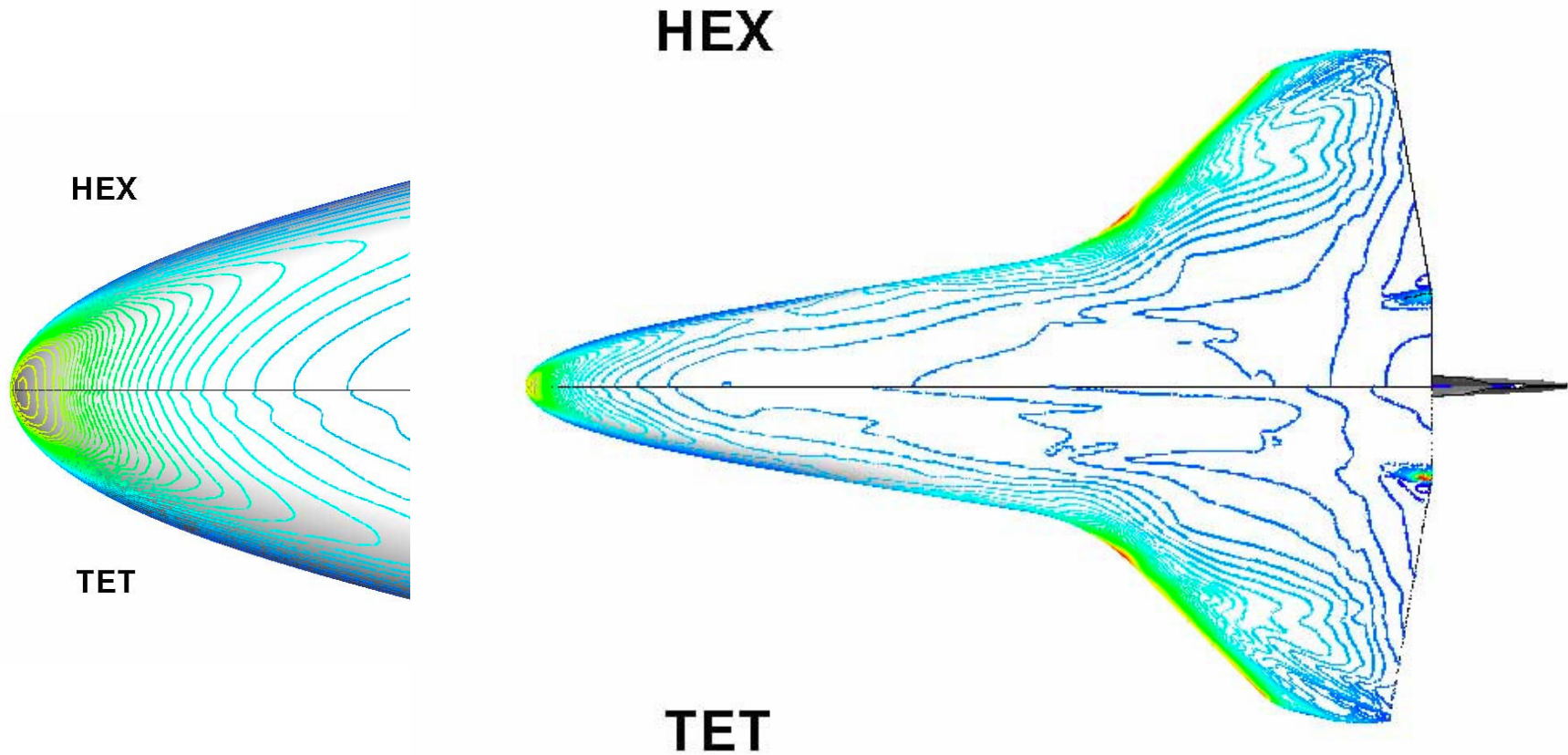
STS-2 Mach 24 -- Windside Surface Heating



STS-2 Mach 24 -- Fuselage Surface Heating



STS-2 Mach 24 -- Surface Heating Contours



Future Plans

- Update io consistent with version 11
- Resolve / understand symmetry plane issues
- Resurrect turbulence models
- Engage the adjoint for grid adaptation
- Engage PHYSICS_MODULES currently in LAURA for
 - Free-energy minimization
 - Coupled radiation using HARA
 - Coupled ablation

