FUN3D v13.4 Training

Session 16: Aeroelastic Simulations

Kevin Jacobson

Session Scope

- What this will cover
  - The two methods of aeroelastic coupling with FUN3D
    - Static coupling with an external structural solver (linear or nonlinear structures)
    - Dynamic coupling to a self-contained, mode-based, linear structures model
  - Gust response simulations
- What will not be covered
  - Projection of mode shapes and forces/displacements to/from CFD and FEM
  - Structural modeling or FEM usage
- What should you already be familiar with
  - Basic steady-state, time-dependent, and dynamic-mesh solver operation and control, especially as pertains to deforming meshes

Introduction

- Background
  - Aeroelastic problems of interest that can be tackled with FUN3D fall into 2 general categories
    - Static: structural displacement asymptotes to a fixed level; coupling between CFD and CSD can be done infrequently - typically interested in accounting for the structural displacement on (say) cruise performance
    - Dynamic: the change in aero affects the structural deformation to the extent that there is an unsteady coupling between the two; coupling between CFD and CSD must be done frequently - prediction of flutter onset is the classic example
- Compatibility
  - Compatible with incompressible/compressible flow; mixed elements; 2D/3D
- Status
  - Modal (flutter) analysis fairly routine; static FEM coupling much less so; capability for dynamic FEM under development

Static Aeroelastics - Overview

- Basic process (*not* a **`moving_grid`** problem - no **`moving_body.input`**)
  1. Solver starts with an initial grid and solution
  2. Solver reads in a new surface shape and deforms the mesh to fit
  3. Solver performs the requested number of iterations, and outputs aerodynamic loads to a file
  4. Middleware maps aerodynamic loads at CFD grid points onto FEM grid
  5. Structural solver computes new displacements from the airloads
  6. Middleware maps structural displacements onto new surface
  7. Back to step 2; repeat until converged - airloads and displacements
- Historically, Jamshid Samareh of NASA Langley provided middleware ("DDFdrive") for this loads and deflection transfer; release of this software transitioning to FUN3D team – contact FUN3D-Support@lists.nasa.gov
- In principle, the above could be applied every time step of a dynamic aeroelastic case; however, file I/O is very inefficient for this

Static Aeroelastics - New Surface Shape

- Reading of the updated surface(s) is triggered by the CLO **`--read_surface_from_file`**
  - File(s) read once at the start of solver execution (steady-state mode)
  - File root name must be of the form **`[project]_bodyN`** (for body N)
  - File extensions: **`.dat`** or **`.ddfb`**
    - **`[project]_bodyN.dat`** ASCII Tecplot file, "FEPOINT" style
    - **`[project]_bodyN.ddfb`** Binary ("stream") DDFdrive style
    - DDFdrive middleware supports both - **`.ddfb`** preferred
  - File provides new x,y,z coordinates for each surface point plus an integer that identifies the point in the volume-mesh numbering system
  - Options for this *input* surface file input are specified in the **`&massoud_output`** namelist (details later)

Static Aeroelastics - Aero Loads Output

- Output is triggered by the CLO **`--write_aero_loads_to_file`**
  - File(s) written at a user-controlled frequency
  - File root name of the form **`[project]_ddfdrive_bodyN`** (N^{th} body)
  - File extensions: **`.dat`** or **`.ddfb`**
    - **`[project]_ddfdrive_bodyN.dat`** ASCII Tecplot file, "FEPOINT" style
    - **`[project]_ddfdrive_bodyN.ddfb`** Binary ("stream") DDFdrive style
    - DDFdrive middleware supports both
  - File provides current Cp, Cfx, Cfy, Cfz for each surface point plus an identifier that maps the point in the volume mesh
  - Options for this *output* surface file input are specified in the **`&massoud_output`** namelist (next)

Static Aeroelastics - `&massoud_output` (1/2)

- The **`&massoud_output`** namelist serves several closely-related purposes, and the name is not especially well-suited to any of them…
- For static aeroelastics, it is used to
  - Define the aeroelastic body(s) as a collection of boundary surfaces
  - Specify the format of the new surface file and the output aero loads file
  - Specify the frequency of the aero loads output
- Example:

```
&massoud_output
  aero_loads_file_format = 'stream'  (default = 'ascii')
  massoud_file_format    = 'stream'  (default = 'ascii')
  aero_loads_output_freq = -1        (if +n…output every n steps)
  n_bodies               = 1         (default = 0)
  nbndry(1)              = 3         (default = 0)
  boundary_list(1)       = '1,2,3'   (default = '')
/
```

Static Aeroelastics - `&massoud_output` (2/2)

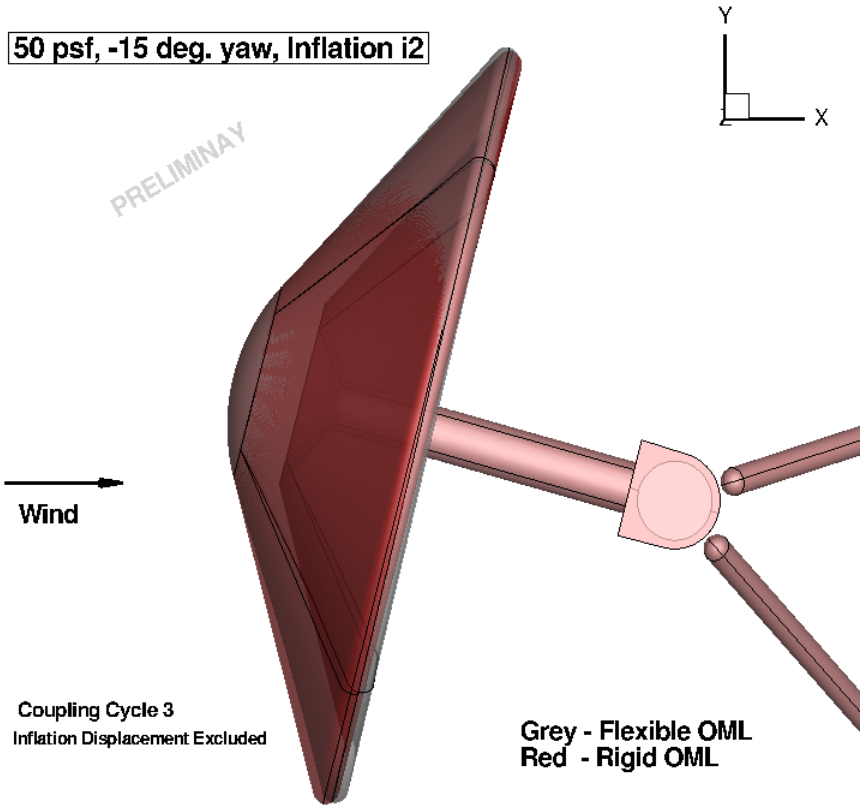
- The **`&massoud_output`** namelist has additional options
  - rotate, translate and scale the geometry written to the aero loads file
  - multiply the aero coefficients by the dynamic pressure to get forces
  - rotate, translate and scale the geometry read from the new surface file
  - output aero loads on either the deflected or undeflected surfaces
  - See Manual for these infrequently-used options

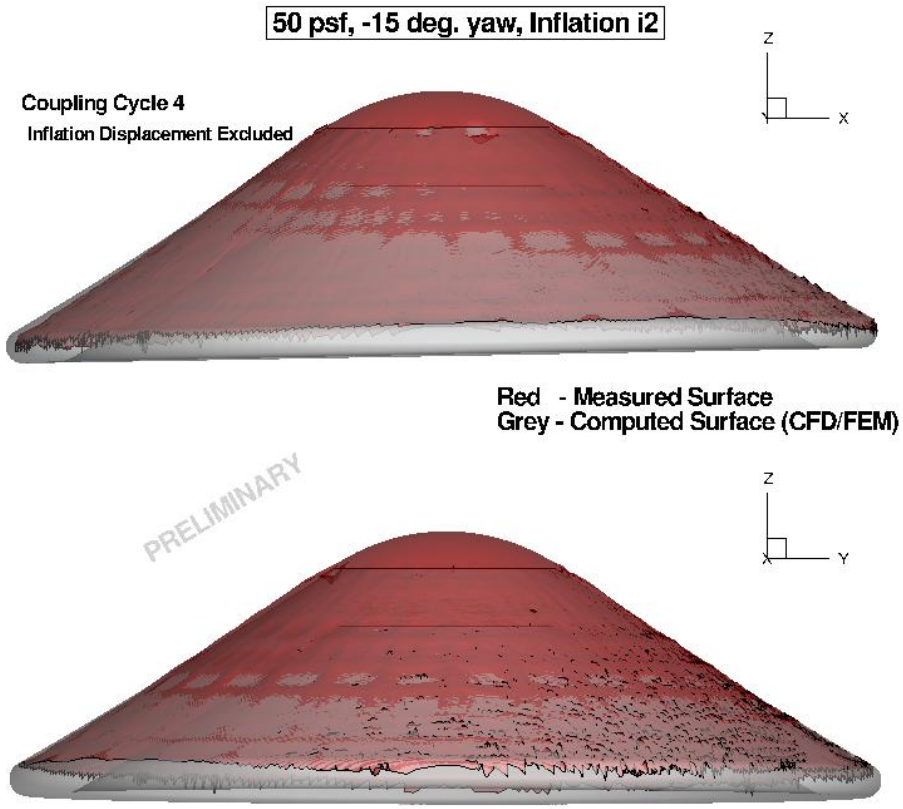
Static Aeroelastics - Towards Automation

- As outlined, the process is rather cumbersome, with multiple separate steady-state runs of the flow solver, the FEM and middleware
  - For our own in-house work we have written a few scripts to orchestrate these steps using DDFdrive
  - Contact FUN3D-Support@lists.nasa.gov if interested (scripts are not part of standard distribution)
- Longer term, we plan on providing interfaces to allow access to coupling data and avoid file I/O
  - Helpful for static coupling with an FEM; essential for dynamic coupling
  - Under development

Static Aeroelastic Coupling Example

Inflatable Decelerator - Low Speed Test





“Bootstrapping” Aeroelastic Problems (1/2)

- All aeroelastic problems, (except highly-specialized rotorcraft problems), utilize either an ASCII Tecplot (.dat) or stream DDFdrive (.ddfb) file to define either a new surface or a set of mode shapes
  - These files need to have the correct surface points for the surface/body in question, plus an integer tag for each point that maps the surface point in the corresponding volume grid.
  - The tag must be preserved throughout any external manipulation of these files (when shape is updated or modes mapped onto surface)
- How does one generate this surface info?
  - Use the CLO **`--write_massoud_file`** and **`&massoud_output`** namelist input during an initial run (perhaps when generating a rigid steady-state solution)
  - This will generate a **`[project]_massoud_bodyN.(dat or ddfb)`** file for input to DDFdrive or as a template for some other middleware.
  - Rename as needed (e.g. **`[project]_bodyN`** for static AE)

“Bootstrapping” Aeroelastic Problems (2/2)

- Example

```
&massoud_output
  n_bodies  = 2
  nbndry(1) = 3
  boundary_list(1) = '5 7 9'
  nbndry(2) = 2
  boundary_list(2) = '3 4'
/
```

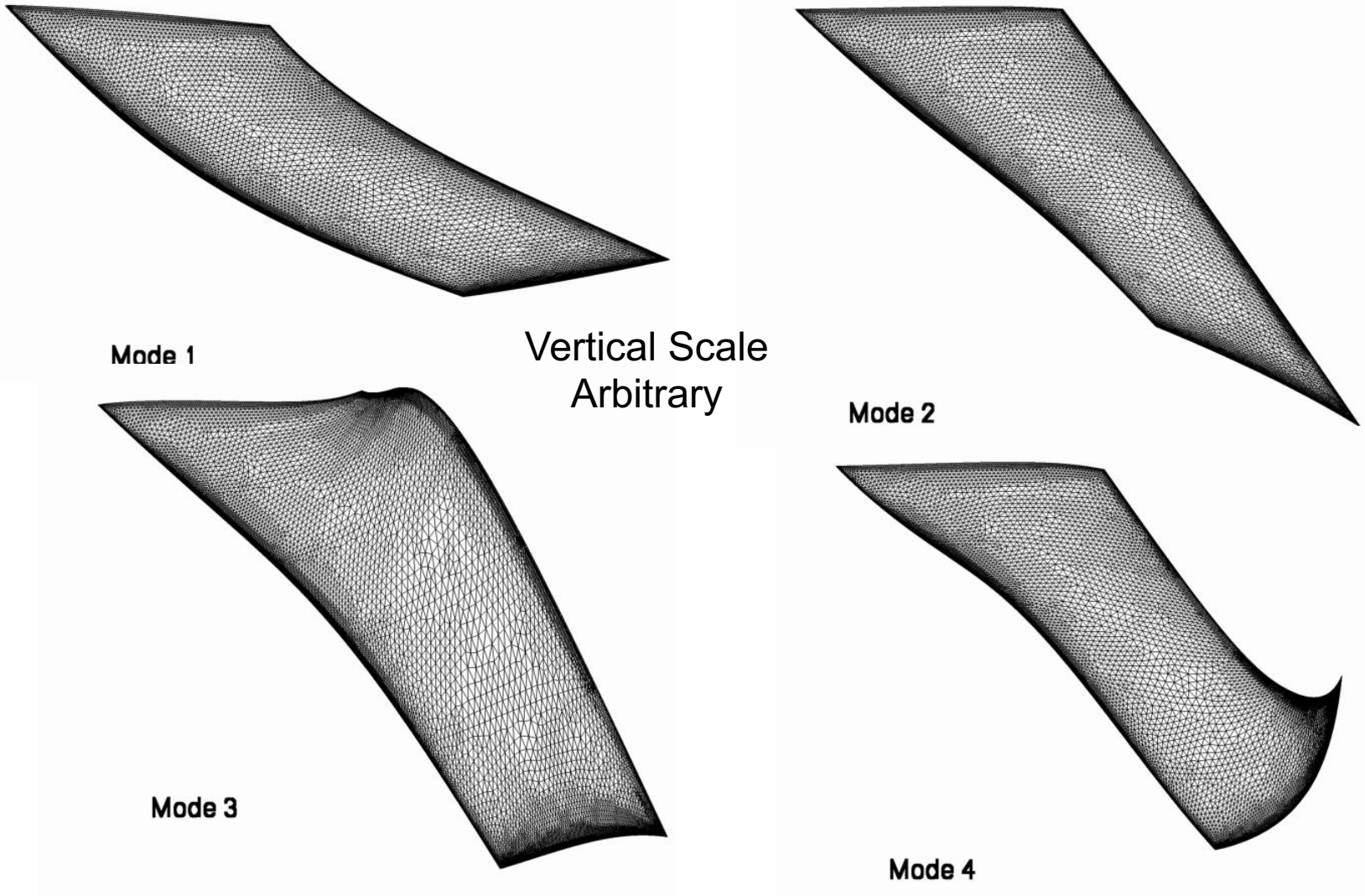
- Also need CLO **`--write_massoud_file`**

Dynamic Aeroelastic Coupling

- For time-accurate aeroelastic modeling, FUN3D currently relies on a modal decomposition approach
  - *Linear* structural dynamics equation (see AIAA 2009-1360) - appropriate for small deflections (e.g., during flutter onset)
  - Deflection assumed a linear combination of eigenmodes (mode shapes)
    - FEM model used a priori to extract eigenmodes / frequencies
    - Typically only a limited set of the “important” eigenmodes retained
  - A *nonlinear* aerodynamics model is used (FUN3D), so effects of shocks and viscosity can be captured in the flow field
  - Middleware (e.g., DDFdrive) maps eignenmodes onto CFD surface in a one-time preprocessing step; at startup FUN3D reads these
  - Aerodynamics at current time step determine the weight applied to each eigenmode; current shape is weighted sum of eigenmodes

Dynamic Aeroelastic Coupling

First 4 Mode Shapes AGARD 445 Wing



Dynamic Aeroelastic Coupling

- Typical flutter assessment process
  1. Run FEM to extract and output the desired modes
  2. Run FUN3D in steady-state mode with **`--write-massoud`** CLO to generate a steady-state solution and provide a file(s) that will serve as a template for subsequent mode-shape files
  3. Map the FEM modes onto the template (DDFdrive can be used) to generate one surface file per mode
  4. Run FUN3D in moving-grid, time-dependent mode, using modal aeroelastic inputs (upcoming slides) with critical damping ratio ~1
     - This yields a static aeroelastic deflection, the starting point for flutter assessment
     - Symmetric configuration at zero AoA can skip this step (as in the case in tutorial example covered later)
  5. Run FUN3D in moving-grid, time-dependent mode, using modal aeroelastic inputs with a initial perturbation to “kick” elastic response; does response grow or decay?

Dynamic Aeroelastic Coupling

- Steps 4&5 require command-line "option": **`--aeroelastic_internal`**
- File nomenclature / format for mode shape input files
  - For every aeroelastic body B, each mode shape M is in a different file: **`[project]_bodyB_modeM.dat (.ddfb)`**
  - Files are once again either ASCII Tecplot files (**`.dat`**) or stream DDFdrive files (**`.ddfb`**), similar to those input for static aeroelastic analysis, only now have modal amplitudes as well:

```
TITLE="wing-445.6 Mode 1"
VARIABLES= "x" "y" "z" "id" "xmd" "ymd" "zmd"
ZONE  I= 57286 ,  J= 101359 , F=FEPOINT
 0.109050E+01 -0.650348E+00 -0.294021E-01 17  0.000000E+00  0.000000E+00  0.869050E-01
 0.691189E+00 -0.650348E+00  0.000000E+00 18  0.000000E+00  0.000000E+00  0.448300E-01
 0.000000E+00  0.000000E+00  0.000000E+00 23  0.000000E+00  0.000000E+00 -0.276958E-02
```

- Can output a "massoud file" from FUN3D (see "Bootstrapping" slide) to use as a template file with x,y,z, and id to which the middleware can add modal amplitudes

Time Step Size for Aeroelastic Problems

- Identify the **characteristic times** t^*_{chr} for the the various aspect of the problem
  - Structure – natural frequencies of the structural modes
  - Flow:
    - Time it takes for a fluid particle to travel a characteristic length of the body
    - Shedding or DES frequency if applicable
- Find step size for each characteristic time, Δt_{struct}, Δt_{flow}, Δt_{DES} , …
  - $\Delta t = t_{chr}/N$ where $N \geq 100$
- Typically want the <u>minimum</u> time step computed from your relevant physics
  - For low frequency motion, the time it takes a fluid particle to travel a characteristic length of the body may drive your time step selection.
  - Otherwise, you may have poor subiteration convergence, instability, etc.

Additional Considerations

- Be especially careful with dimensions and coordinate systems since at one point or another exchange must be done between CFD and FEM - need to ensure consistency!
- Note that frequencies increase in the higher modes; choose time steps accordingly

Tutorial Case: AGARD 445 Wing (1/8)

- Test case located in: tutorials/flow_modal_aeroelasticity
  - **`run_tutorial.sh`** script performs steps 2,3, and 5 of the typical flutter assessment process
    - FEM mode shapes (Step 1) are given in Modes/445.6-mode.dat
    - No need for Step 4: symmetric airfoil at 0 deg. AoA
    - This tutorial case takes several hours to run
- Well-known test case for flutter prediction
  - Tested in NASA Langley Transonic Dynamics Tunnel c. 1960
  - Often run as inviscid (as we do here)
  - Typically run over a range of transonic Mach numbers to see at what dynamic pressure the wing begins to flutter (and with what frequency): here we consider only Mach 0.9 and q = 75 psf

Tutorial Case: AGARD 445 Wing (2/8)

- Step 2: Generate template for FUN3D mode-shape files
  - Typical steady-state run, but with CLO **`--write_massoud_file`**, and fun3d.nml namelist input:

```
&massoud_output
  n_bodies          = 1
  nbndry(1)         = 1    ! Note:family lumping -> 1 boundary
  boundary_list(1)  = '3'  ! Lumped wing is now boundary no. 3
/
```

  - Generates file wing-445.6_massoud_body1.dat:

```
title="surface points and l2g id for massoud"
variables="x","y","z","id"
zone t="mdo body 1", i=50827, j=101359, f=fepoint,  solutiontime= 0.8000000E+03,
strandid=0
   0.294576800000000E+001 -0.250000000000000E+001  0.212627299999966E-001          1
   0.386499999999999E+001 -0.250000000000000E+001  0.000000000000000E+000          2
   0.254080100000000E+001 -0.209625900000000E+001  0.230393900000010E-001          3
   0.222790400000000E+001 -0.209625900000000E+001  0.000000000000000E+000          4
   ...
```

  - FUN3D mode files must preserve these x,y,z *and* id values, and append the x,y,z modal amplitude at the end of each line – Mode.f does this

Tutorial Case: AGARD 445 Wing (3/8)

- Step 3: Map FEM modal data onto template file generated in Step 2 (one file per mode). In this case we use the custom code Mode.f but could alternatively use a more general tool like DDFdrive
  - In this case we end up with 4 files, e.g. **`wing-445.6_body1_mode1.dat`**

```
TITLE="wing-445.6 Mode 1"
VARIABLES= "x" "y" "z" "id" "xmd" "ymd" "zmd"
ZONE  I=       50827 ,  J=      101359 , F=FEPOINT
 0.294577E+01 -0.250000E+01  0.212627E-01     1  0.000000E+00  0.000000E+00  0.182049E+01
 0.386500E+01 -0.250000E+01  0.000000E+00     2  0.000000E+00  0.000000E+00  0.239954E+01
 0.254080E+01 -0.209626E+01  0.230394E-01     3  0.000000E+00  0.000000E+00  0.131437E+01
 0.222790E+01 -0.209626E+01  0.000000E+00     4  0.000000E+00  0.000000E+00  0.114554E+01
 ...
```

  - Mode.f has lost a few digits of precision relative to the template, but otherwise preserves the x,y,z and id values; xmd, ymd, and zmd are the mode amplitudes at each point

Tutorial Case: AGARD 445 Wing (4/8)

- Step 5: **`moving_body.input`** file:

```
&body_definitions
  n_moving_bodies    = 1                ! define bodies as collection of surfaces
  body_name(1)       = 'airfoil'        ! some name
  n_defining_bndry(1) = -1              ! use all solid surfaces
  motion_driver(1) = 'aeroelastic'
  mesh_movement(1) = 'deform'
/
&aeroelastic_modal_data  ! below, b = body #, m = mode number
  plot_modes    = .true.     ! can tecplot to verify mode shapes read correctly
  nmode(1)      = 4          ! 4 modes for this body
  uinf(1)       = 973.4      ! free stream velocity (ft/s)
  grefl(1)      =   1.00       ! scale factor between CFD and FEM models
  qinf(1)       =  75.0        ! free stream dynamic pressure, psf
  freq(1,1)     =  60.3135016  ! mode frequency (rad/s)
  freq(2,1)     = 239.7975647
  freq(3,1)     = 303.7804433
  freq(4,1)     = 575.1924565
  gmass(1:4,1) = 4*0.08333  ! generalized mass (nondim)
  gvel0(1:4,1) = 4*0.1      ! nonzero initial velocity to kick off dynamic
                           ! response; set = 0 on restart - don't kick
 /                         ! me twice
```

Tutorial Case: AGARD 445 Wing (5/8)

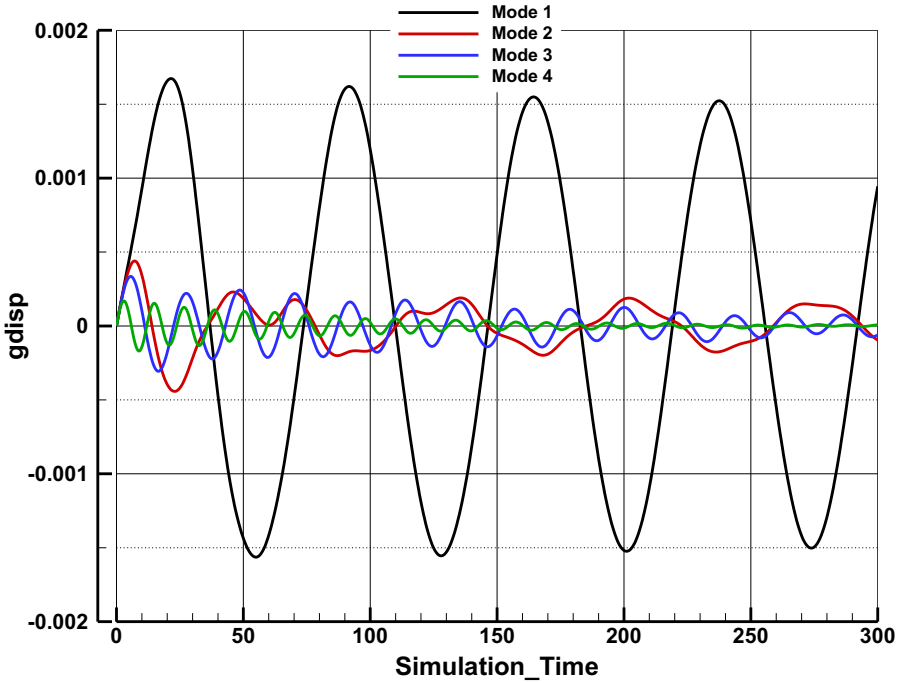
- Step 5 (cont) Setting the FUN3D timestep
  - From experiment, the flutter frequency at Mach 0.9 is ω^* ~ 120 rad/sec, so we'll assume we need to resolve at least up to this frequency
  - From nondimensionalization slides, have
    - $t_{chr} = (1/f^*)\, a^*_{inf}\, (L_{ref}/L^*_{ref}) = (2\pi/\omega^*)\, a^*_{inf}\, (L_{ref}/L^*_{ref})$
    - $\Delta t = t_{chr}/N$
  - Take 200 steps to resolve this frequency; from previous slide have
    - U^*_{inf} = 973 ft/sec so at M=0.9, a^*_{inf} = 1081 ft/sec
    - The grid is in ft so $L_{ref}/L^*_{ref} = 1$
    - $\Delta t = (6.28/120)\, 1081\, (1) / 200 = 0.283$ (tutorial uses 0.3)
    - In practice, would need to do a time step refinement to verify this time step is adequate (at this time step, mode 4 resolved with only ~42 steps/period)

Tutorial Case: AGARD 445 Wing (6/8)

- Output of generalized force, displacement and velocity into files, e.g. **`aehist_bodyN_modeM.dat`** (ASCII Tecplot)

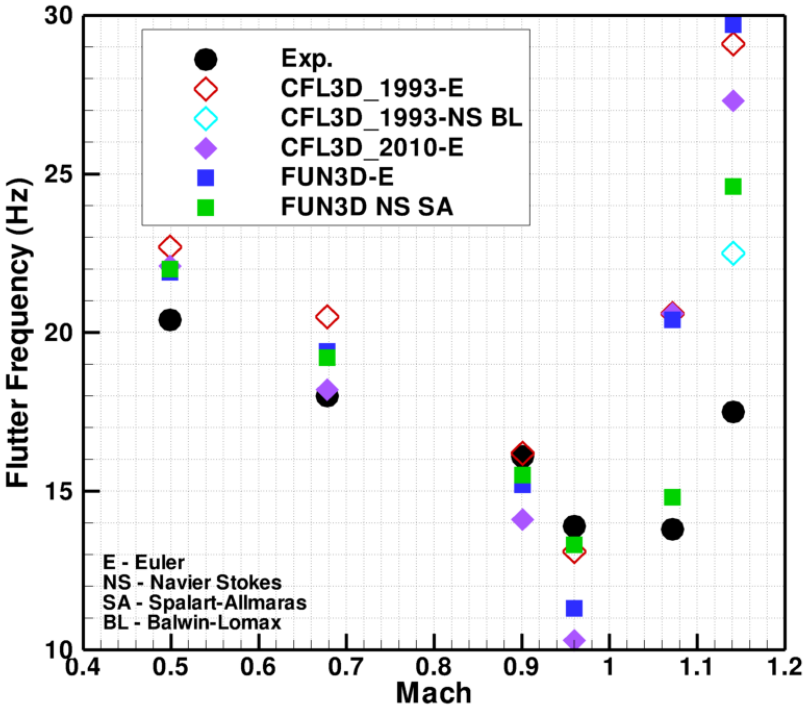
```
#  qinf =  7.50000E+01  uinf =  9.73400E+02  Mach =  9.00000E-01
variables = "Simulation_Time", "gdisp", "gvel", "gforce"
zone t = "modal history for airfoil, mode   1"
    0.00000000E+00    0.00000000E+00    1.00000000E-01    0.00000000E+00
    3.00000000E-01    2.77176987E-05    9.98502122E-02   -8.15943032E-02
    6.00000000E-01    5.53732953E-05    9.95522312E-02   -7.22530082E-02
   ...
```

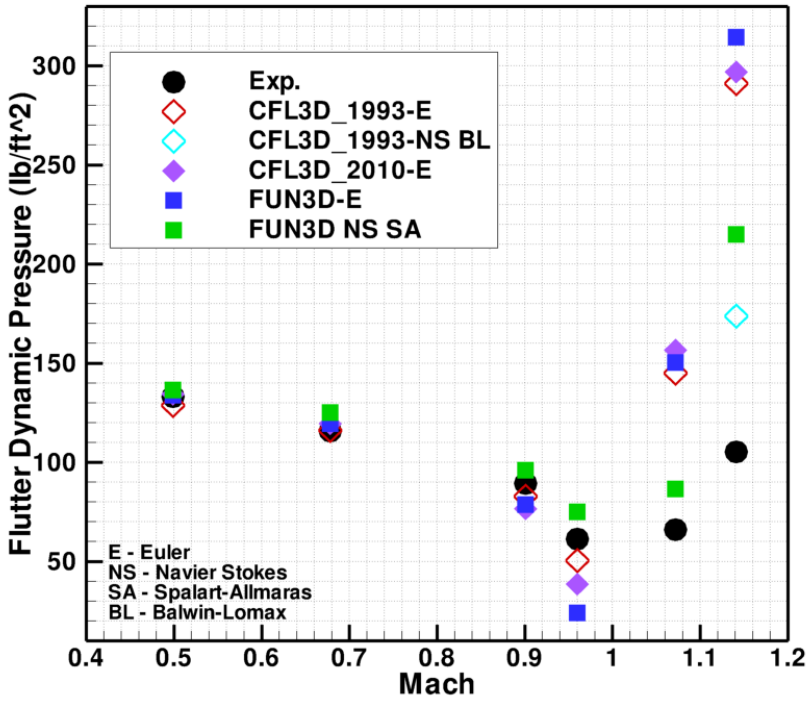
Typical plot to assess dynamic response to disturbance (recall initial 0.1 perturbation in gvel)
At this q, response damps very slowly



Tutorial Case: AGARD 445 Wing (7/8)

- The dynamic pressure (q = 75 psf) in the tutorial does not lead to flutter at M = 0.9 – so we would need to increment q and repeat until we found a response that grows with time (M = 78.6 psf) – then repeat over the Mach range
- Pawel Chwalowski, Aeroelasticity Branch, NASA Langley has carried out this exercise and provided these plots (not part of tutorial):

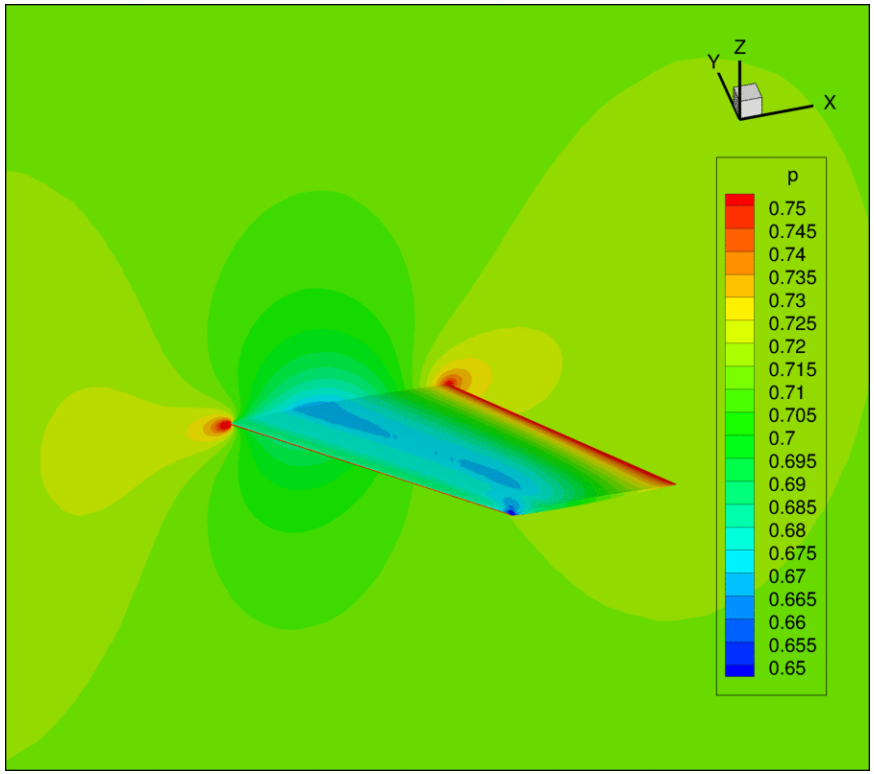


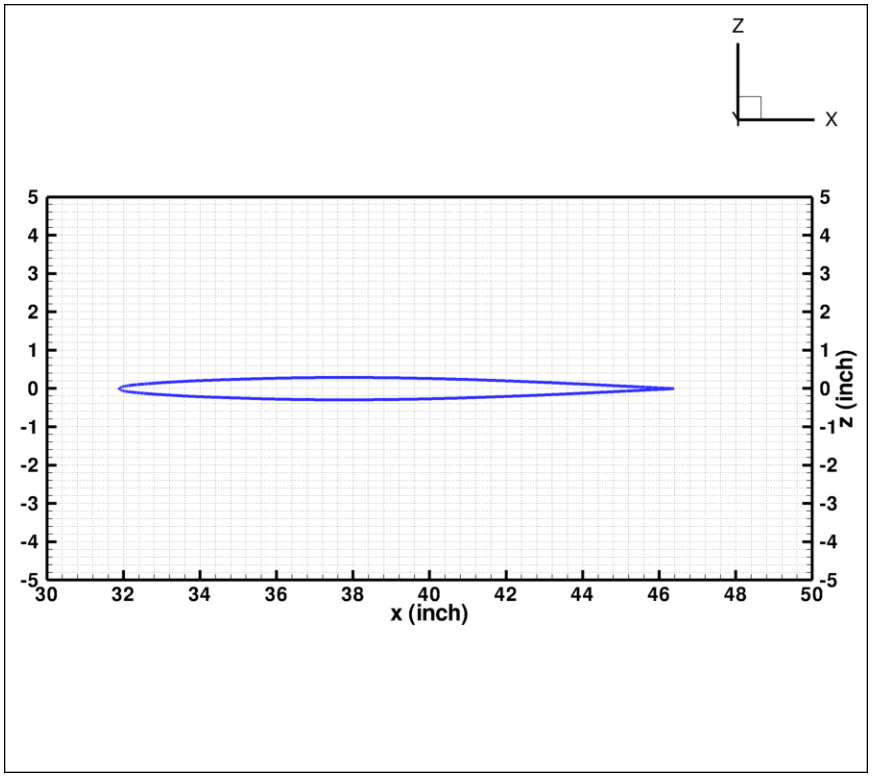


Tutorial Case: AGARD 445 Wing (8/8)

Results Courtesy Pawel Chwalowski, Aeroelasticity Branch, NASA Langley
(These animations not generated as part of the tutorial)

Inviscid Flow Mach=0.9, Flutter condition, Q = 78.6 psf





Gust Simulations (1/5)

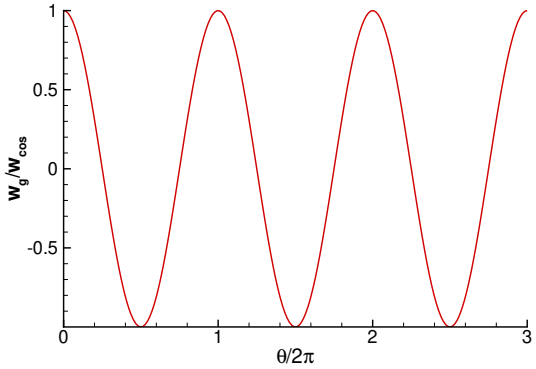
- NASA/TM–2012-217771 serves as the FUN3D manual for gust analysis
- Gusts are modeled in FUN3D with the field velocity method
  - Modifies the grid velocity with the gust contribution

$$\dot{x}\hat{i} + \dot{y}\hat{j} + \dot{z}\hat{k} = (\dot{x}_0 - u_g)\,\hat{i} + (\dot{y}_0 - v_g)\,\hat{j} + (\dot{z}_0 - w_g)\,\hat{k}$$

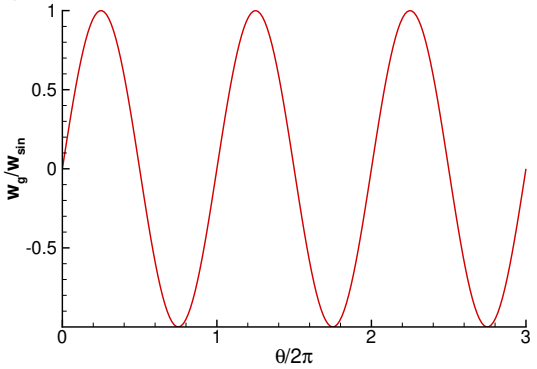
  - Does not change the displacements
  - Not applied to surface nodes
- Compatibility
  - Compatible with compressible flow; mixed elements; 2D/3D
- Gusts propagate in the positive x-direction at the freestream Mach number and are uniform in the planes normal to x

Gust Simulations (2/5)

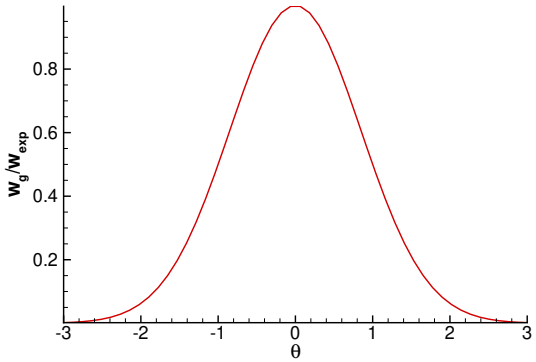
- Gust profiles are formed from four elementary profiles



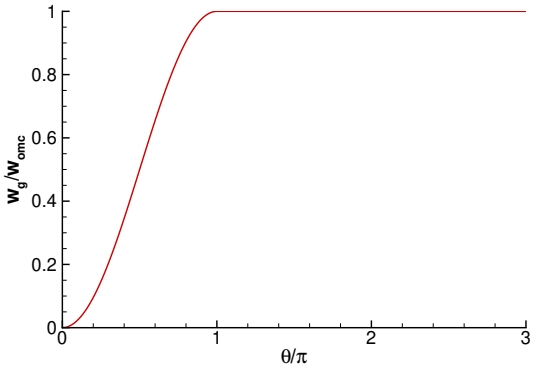
Sine



Cosine



Gaussian pulse



1 - Cosine

- Use superposition to form complex gust profiles
- Parameters of gust components controlled with the **`gust_data`** namelist

Gust Simulations (3/5)

- Parameters of gust components controlled with the &**gust_data** namelist

```
&gust_data
    X0_gust = 0.0  ! x starting location of for all gusts
```

- Sine and Cosine gusts

$$w_g(x,t) = w_{sin} sin\theta \qquad w_g(x,t) = w_{cos} cos\theta$$

$$\theta = \frac{2\pi\tau M_\infty}{L_{g\,sin}} \quad for \quad \tau > 0 \qquad \tau = t - t_{ref\,sin} - \frac{(x - x_0)}{M_\infty}$$

```
&gust_data
    ngust_sin = 1              ! Number of sine profiles
    l_gust_sin(1) = 1.0        ! Wave length
    tref_gust_sin(1) = 1.0     ! Start time
    u_gust_sin(1) = 0.0        ! x velocity magnitude
    v_gust_sin(1) = 0.0        ! y velocity magnitude
    w_gust_sin(1) = 0.05       ! z velocity magnitude
```

- Replace ***_sin** namelist parameters with ***_cos** for cosine gust

Gust Simulations (4/5)

- Gaussian profile

$$w_g(x,t) = w_{exp} e^{-c\theta^2} \qquad c = ln(2)$$

$$\theta = \frac{\tau M_\infty}{L_{g\,exp}} \qquad \tau = t - t_{ref\,exp} - \frac{(x - x_0)}{M_\infty}$$

```
&gust_data
    ngust_exp = 1            ! Number of Gauss profiles
    l_gust_exp(1) = 1.0      ! Half-height length
    tref_gust_exp(1) = 1.0 ! Reference time (max velocity mag.)
    u_gust_exp(1) = 0.0      ! x velocity magnitude
    v_gust_exp(1) = 0.0      ! y velocity magnitude
    w_gust_exp(1) = 0.05     ! z velocity magnitude
```

Gust Simulations (5/5)

- 1-Cosine profile

$$w_g(x,t) = \frac{1}{2} w_{omc} \left[1 - cos\theta\right]$$

$$\theta = \frac{\pi \tau M_\infty}{L_{g\,omc}} \quad for \quad 0 < \tau < \frac{L_{g\,omc}}{M_\infty}$$

$$\theta = \pi \quad for \quad \tau \geq \frac{L_{g\,omc}}{M_\infty}$$

$$\tau = t - t_{ref\,omc} - \frac{(x - x_0)}{M_\infty}$$

```
&gust_data
    ngust_omc = 1              ! Number of 1-cos profiles
    l_gust_omc(1) = 1.0        ! Length of profile (half cosine
                                 wave length)
    tref_gust_omc(1) = 1.0 ! Start time
    u_gust_omc(1) = 0.0        ! x velocity magnitude
    v_gust_omc(1) = 0.0        ! y velocity magnitude
    w_gust_omc(1) = 0.05       ! z velocity magnitude
```

- Can form a full 1-cosine profile with two components
  - The second has equal but negative magnitude and starts at t_{ref} (2) = $\frac{L_{g\,omc}}{M_\infty}$

Additional Gust Considerations

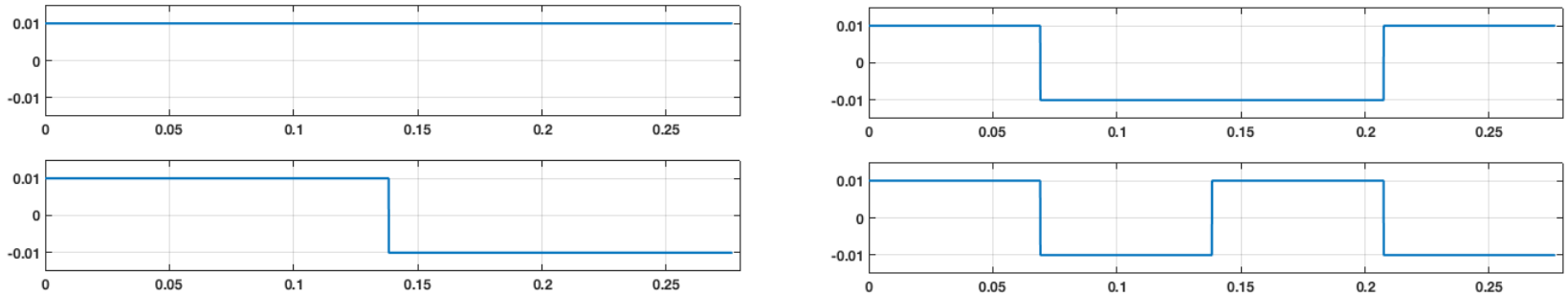
- Gust reference times and velocity magnitudes are nondimensional (Mach number for velocity)
- Consider gust period in addition to the flow and structural frequencies when calculating your time step
- Note the difference the definition of θ between the cosine and 1-cosine gust means the wavenumber is different for the same **`1_gust_*`** value

Reduced-order Models (1/2)

- Aeroelastic analysis based on FUN3D produces transient response data
  - Relatively slow to explore a given parameter space
- Reduced-order modeling (ROM) is one approach to leverage more accurate CFD yet produce linear-aeroelasticity-type data (root-locus plots)
  - Can lead to better understanding of the physics especially when there are multiple flutter mechanisms
  - Once the ROM is formed, it can rapidly produce results and explore a parameter space
    - Takes **minutes compared to hours or days** per CFD simulation
  - Process:
    1. Perform aeroelastic FUN3D simulations with input excitations to form impulse responses
    2. Generate aerodynamic state-space model from impulse responses
    3. Combine with state-space model of structures to form reduced-order aeroelastic system

Reduced-order Models (2/2)

- AEROM – nonintrusive ROM software from NASA Langley
  - Utilizes Walsh functions to perturb multiple inputs within a single FUN3D simulation



  - Usage will not be covered here
  - Contact Walter Silva (walter.a.silva@nasa.gov) for more information
- Other ROM considerations
  - A ROM may lose accuracy as a representation of the CFD as you venture away from the conditions used to generate the ROM
  - More detailed training on ROMs will be provided in “A Tutorial on a Unified Approach for Computational Aeroelasticity” at SciTech 2019

List of Key Input/Output Files

- Beyond basics like **`fun3d.nml`**, **`[project]_hist.tec`**, etc.:
- Input
  - **`moving_body.input`**
  - **`[project]_body1.dat (.ddfb)`** (external FEM / static AE)
  - **`[project]_bodyB_modeM.dat (.ddfb)`** (modal structures)
- Output
  - **`aehist_bodyB_modeM.dat`** (modal structures only)
  - **`[project]_ddfdrive_bndryN.dat`** (with CLO)