

# **FUN3D v12.4 Training**

## **Session 17:**

# **Rotorcraft Simulations**

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# Session Scope

- What this will cover
  - Overview of actuator-disc models for rotorcraft
  - Overview of setup for overset, articulated-blade rotorcraft simulations
    - Rigid Blades
    - Elastic Blades / Loose Coupling to Rotorcraft Comprehensive Codes
- What will not be covered
  - Rotorcraft Comprehensive Code set up and operation
  - All the many critical setup details
- What should you already know
  - Basic time-accurate and dynamic-mesh solver operation and control
  - Rudimentary rotorcraft aeromechanics (collective, cyclic...)



# Introduction

- Background
  - FUN3D can model a rotor with varying levels of fidelity/complexity
    - As an actuator disk - when only the overall rotor influence is needed
    - As rotating, articulated-blade system (cyclic pitch, flap, lead-lag), with or without aeroelastic effects - if detailed airloads are needed
  - Trim and aeroelastic effects require coupling with a rotorcraft “comprehensive” code
  - As a steady-state problem for rigid, isolated, fixed-pitch blades in a rotating noninertial frame (not covered here)
- Compatibility
  - Coupled to the CAMRAD II and RCAS comprehensive codes
- Status
  - Coded for multiple rotors, but largely untested
  - Far less experience / testing with RCAS than with CAMRAD II



# Time-Averaged Actuator-Disk Simulations (1/2)

- Actuator disk method utilizes momentum/energy source terms to represent the influence of the disk (pressure jump)
  - Original implementation by Dave O'Brien (GIT Ph.D. Thesis)
  - HI-ARMS implementation (SMEMRD) by Dave O'Brien ARMDEC adds trim and ability to use C81 airfoil tables (*Not covered*)
- Simplifies grid generation – disk is embedded in computational grid (note some refinement in the vicinity of actuator surface needed for accuracy)
- Any number of actuator disks can be modeled
- Different disk loading models available
  - **RotorType** = 1 actuator disk
    - **LoadType** = 1 constant (specified thrust coefficient  $C_T$ )
    - **LoadType** = 2 linearly increasing to blade tip (specified  $C_T$ )
    - **LoadType** = 3 blade element based (computed  $C_T$ )
  - **RotorType** = 2 actuator blades (time-accurate) **Not Functional**

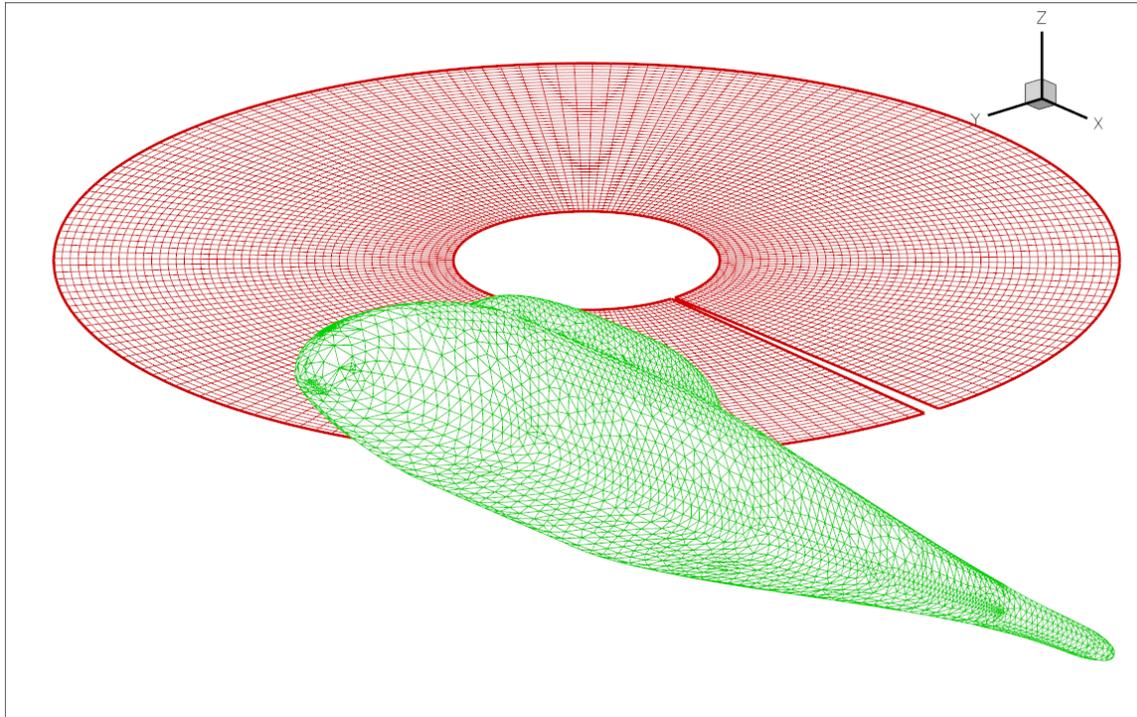


# Time-Averaged Actuator-Disk Simulations (2/2)

- Actuator disk implementation runs orthogonal to the standard steady-state flow solver process (compressible and incompressible)
  - Standard input grid formats for the volume grids
  - Standard solver input deck (`fun3d.nml`)
  - Standard output is available (`project.forces`, `project_hist.tec`, `project_tec_boundary.plt`)
  - Want similar solution convergence as a standard steady-state case
- Actuator disk model is activated in the command line by `mpirun nodet_mpi --rotor`
  - Rotor input deck file (`rotor.input`) is required in the local directory
  - `rotor.input` contains disk geometry and loading specifications
  - The disk geometry and loading are output in plot3d format in files `source_grid_iteration#.p3d` and `source_data_iteration#.p3d`



# Incompressible Robin/Actuator Disk



Advance Ratio = 0.051 ( $V_{\infty}/V_{tip}$ )  
Thrust coefficient  $C_T = 0.0064$   
Angle of attack = 0 deg  
Shaft angle = 0deg



# rotor.input File

- Constant/linear loading needs only a subset of the data in the file

```

# Rotors      Uinf/Uref  Write Soln  Force Ref  Moment Ref  ! Below we set Uref = Uinf
      1          1.000      1500      0.001117   0.001297   ! Adv Ratio = Uinf/Utip
=== Main Rotor ===== ! So here Utip/Uref = 1/AR
Rotor Type   Load Type   # Radial   # Normal   Tip Weight
      1           2           50         180         0.0
X0_rotor     Y0_rotor     Z0_rotor     phi1        phi2        phi3
      0.696       0.0         0.322       0.00        -0.0        0.00
Utip/Uref    ThrustCoff   PowerCoff    psi0   PitchHing/R   DirRot
      19.61       0.0064     -1.00        0.0         0.0         0
# Blades     TipRadius   RootRadius  BladeChord  FlapHinge/R  LagHinge/R
      4           0.861       0.207       0.066       0.051       0.051
LiftSlope    alpha, L=0   cd0          cd1          cd2
      0.0         0.00       0.002       0.00        0.00
CL_max       CL_min       CD_max       CD_min       Swirl
      0.00        0.00       0.00        0.00        0
Theta0       ThetaTwist   Thetals     Theta1c     Pitch-Flap
      0.0         0.00       0.0         0.0         0.00
# FlapHar    Beta0        Betals      Beta1c
      0           0.0         0.0         0.0
Beta2s       Beta2c       Beta3s      Beta3c
      0.0         0.0         0.0         0.0
# LagHar     Delta0       Deltals    Delta1c
      0           0.0         0.0         0.0
Delta2s      Delta2c      Delta3s     Delta3c
      0.0         0.0         0.0         0.0

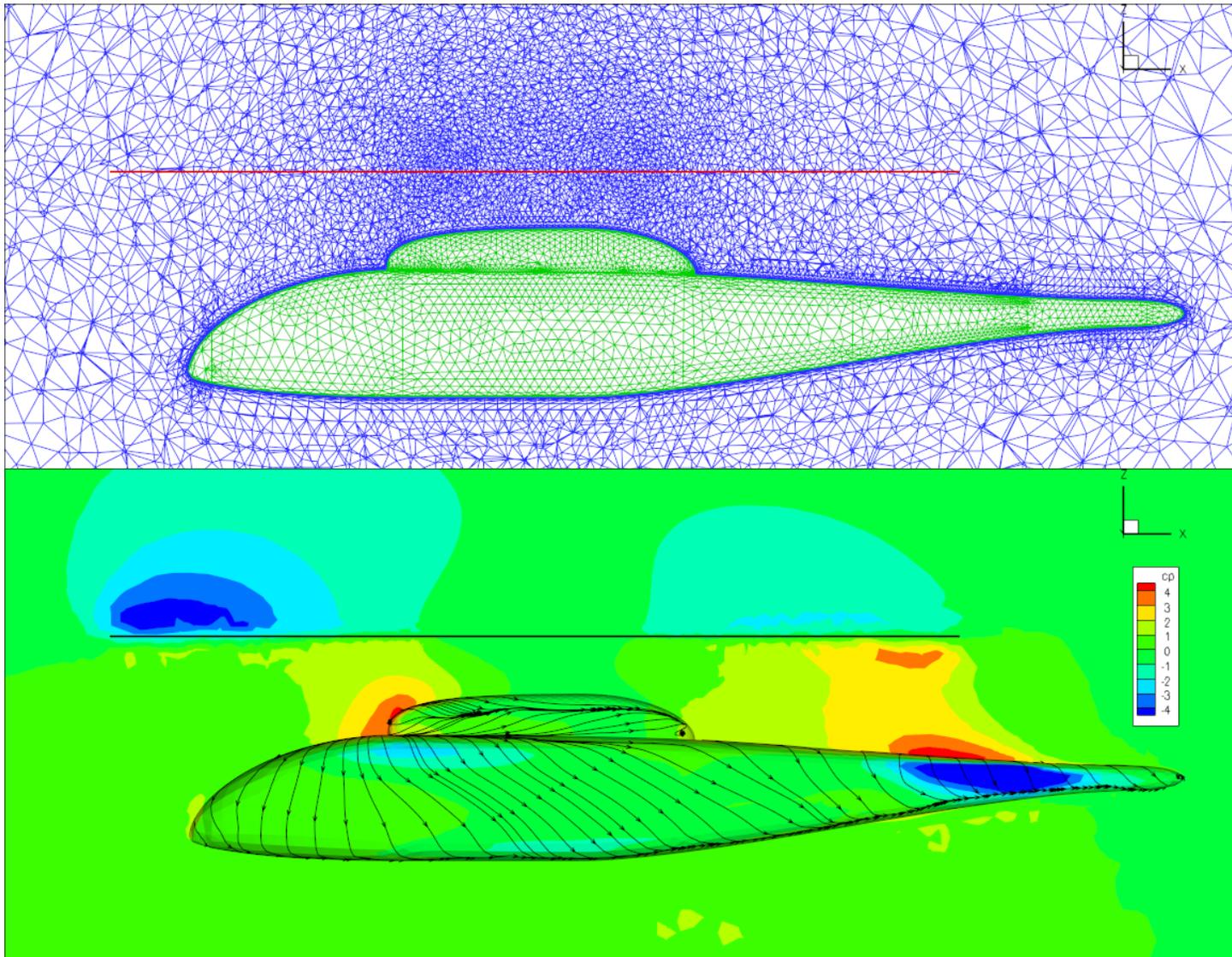
```

Key:  
Required for constant loading  
Required for blade element  
 Not implemented  
 (all must have a values)

- Note  $V_{ref}=V_{tip}$  is bad choice for incompressible flow - suggest using rotor induced velocity



# Incompressible Robin/Actuator Disk



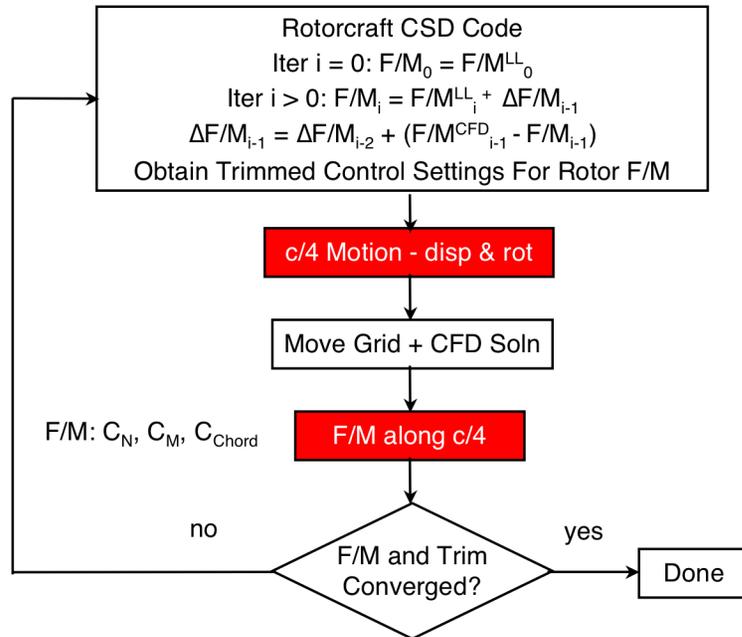
# Articulated-Blade Simulations

- Relies on the use of overset grids; blades may be rigid or elastic
- Elastic-blade cases (or *trimmed* rigid-blade cases) must be coupled to a rotorcraft Computational Structural Dynamics (CSD, aka comprehensive) code such as CAMRAD or RCAS
  - The CSD code provides trim solution in addition to blade deformations
  - The interface to the CSD code is through standard OVERFLOW `rotor_N.onerev.txt` and `motion.txt` type files
  - Interface codes for CAMRAD are maintained and distributed by Doug Boyd, NASA Langley (d.d.boyd@nasa.gov)
  - RCAS coupling does not require any interface codes
  - FUN3D has several postprocessing utility codes tailored to CAMRAD
- This is about as complicated as it gets with the FUN3D flow solver
  - There are *many* small details that must be done correctly; we don't have time to cover them all here
  - Novice users of FUN3D will want to start with simpler problems

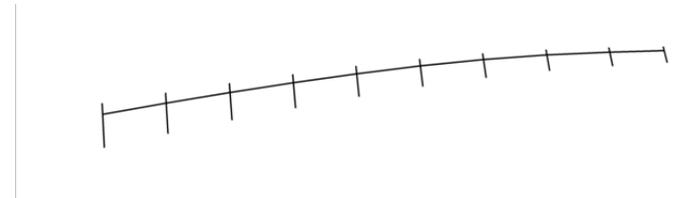


# CFD/CSD – Loose (Periodic) Coupling

## Coupling Process



## CSD -> CFD



## CFD -> CSD



motion.txt and rotor\_onerev.txt files common to FUN3D and OVERFLOW

CFD/CSD loose coupling implemented via shell script with error checking



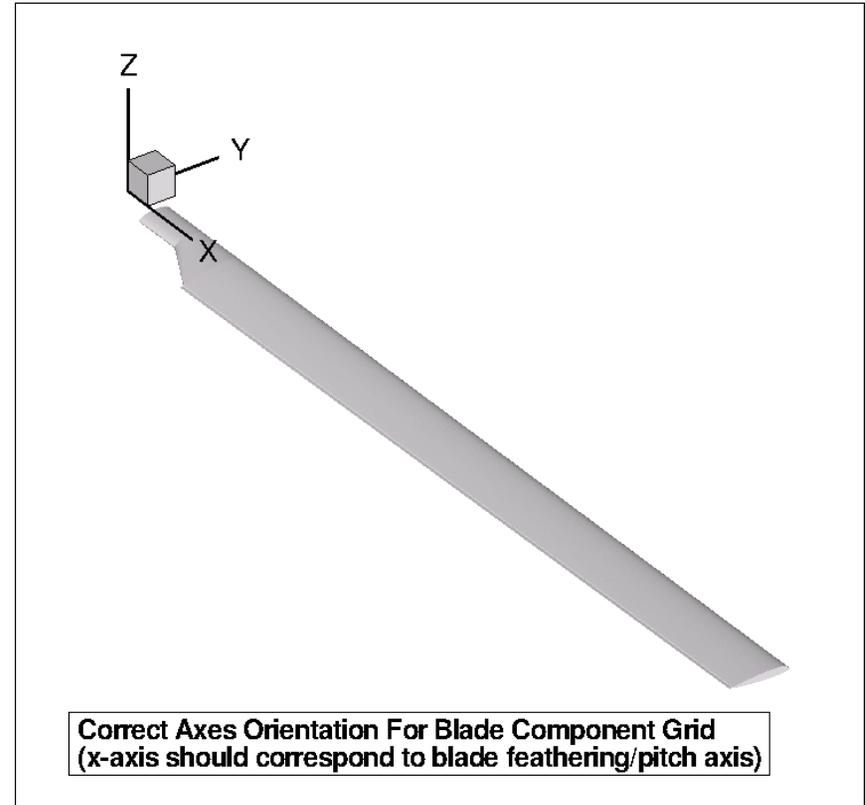
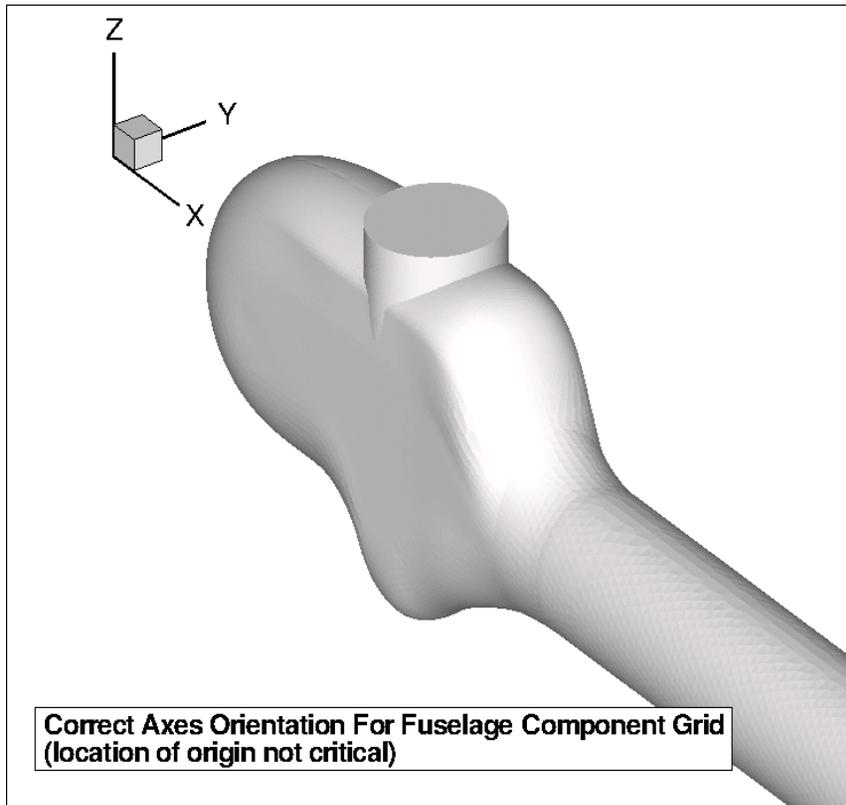
# dci\_gen Preprocessor (1/8)

- A rudimentary code to simplify rotorcraft setup (/utils/Rotorcraft/dci\_gen)
  - Uses libSUGGAR++ routines
  - Takes a single blade grid and a single fuselage / background grid (extending to far field) and assembles them into an N-bladed rotorcraft
  - Creates the SUGGAR++ XML file (**Input.xml\_0**) needed by FUN3D
  - Generates, using libSUGGAR++ calls, the initial ( $t = 0$ ) dci file and composite grid needed by FUN3D
  - Generates the composite-grid “mapbc” files needed by FUN3D
  - Component grids *must* be oriented as shown on following slide
    - Blade must have any “as-built” twist incorporated
    - If grids do not initially meet the orientation criteria, can use SUGGAR++ to rotate them *before* using **dci\_gen**



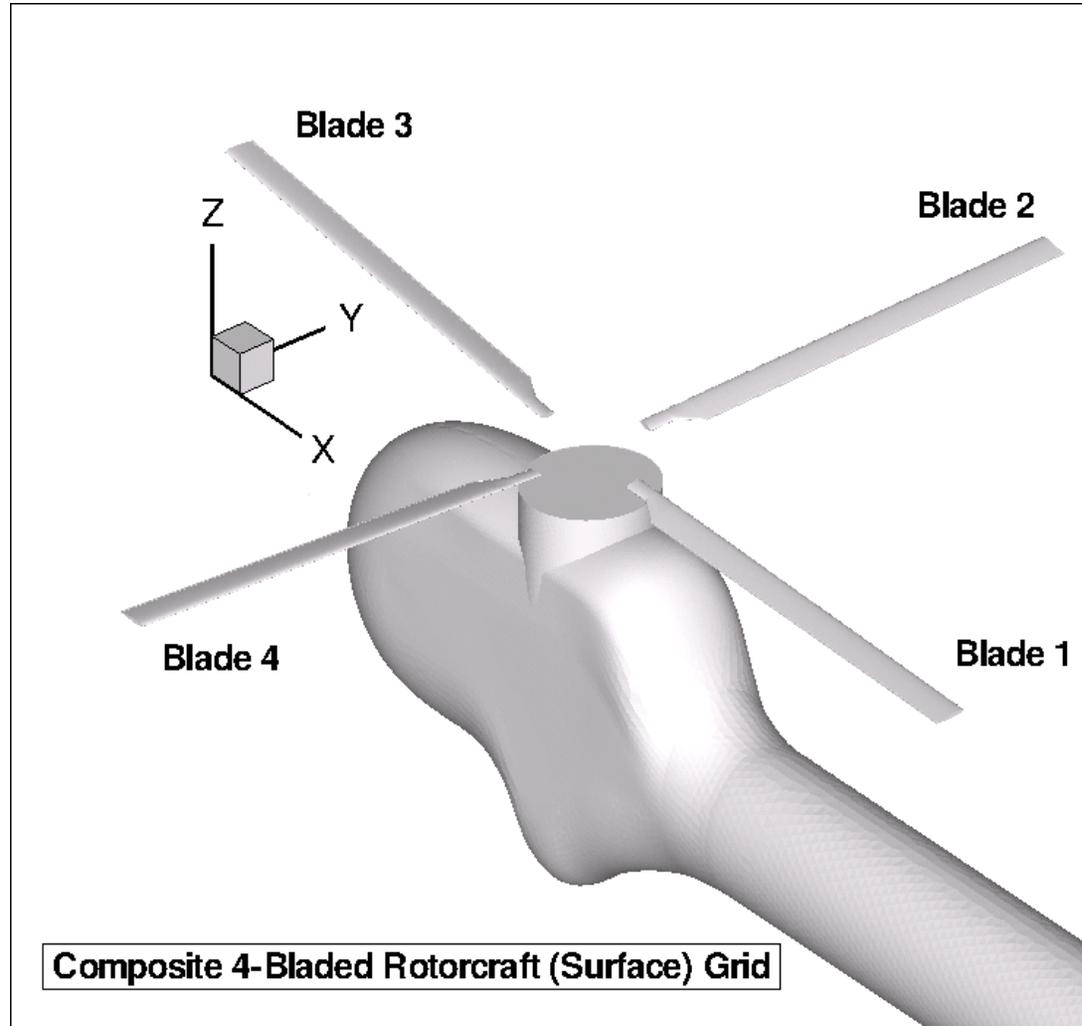
# dcf\_gen Preprocessor (2/8)

## HART II *Component* Grids



# dcgen Preprocessor (3/8)

## HART II *Composite* Grid



# rotor.input File

- Articulated rotors need only a subset of the data (manual defines variables)

```

# Rotors      Uinf/Uref  Write Soln  Force Ref  Mommnt Ref      ! Below we set Uref = Utip
                1          0.245      1500      1.0          1.0          ! Adv Ratio = Uinf/Utip
==== Main Rotor =====
Rotor Type    Load Type    # Radial    # Normal    Tip Weight
                1              1             50          180          0.0
X0_rotor      Y0_rotor      Z0_rotor      phi1         phi2         phi3
                0.0            0.0            0.0          0.00         0.0          0.00
Utip/Uref     ThrustCoff    PowerCoff      psi0        PitchHinge    DirRot
                1.0            0.0064        -1.00         0.0          0.0466        0
# Blades      TipRadius    RootRadius    BladeChord    FlapHinge    LagHinge
                4            26.8330        2.6666        1.741        0.0466        0.0466
LiftSlope     alpha, L=0    cd0           cd1           cd2
                6.28            0.00          0.002         0.00         0.00
CL_max        CL_min        CD_max        CD_min        Swirl
                1.50           -1.50          1.50          -1.50         0
Theta0        ThetaTwist    Thetals       Theta1c       Pitch-Flap
                0.0            0.00          0.0           0.0           0.00
# FlapHar     Beta0         Betals        Beta1c
                0             0.0           0.0           0.0
Beta2s        Beta2c        Beta3s        Beta3c
                0.0            0.0           0.0           0.0
# LagHar      Delta0        Deltals       Delta1c
                0             0.0           0.0           0.0
Delta2s       Delta2c       Delta3s       Delta3c
                0.0            0.0           0.0           0.0

```

Key:  
 Required for rigid and elastic  
 Required for untrimmed rigid  
 Unused (must have a value)



# Nondimensional Input (1/2)

- Typically define the flow reference state for rotors based on the tip speed; thus in `rotor.input`, set  $U_{tip}/U_{ref} = 1.0$  (data line 4)
- This way,  $U_{inf}/U_{ref}$  (data line 1) is equivalent to  $U_{inf}/U_{tip}$ , which is the Advance Ratio, and is usually specified or easily obtained
- Since the reference state corresponds to the tip, the `mach_number` in the `fun3d.nml` file should be the tip Mach number, and the `reynolds_number` should be the tip Reynolds number
- Nondimensional rotation rate: not input directly, but it is output to the screen; you might want to explicitly calculate it up front as a later check:

$$\Omega^* = U_{tip}^* / R^* \text{ (rad/s, } R^* \text{ the rotor radius)}$$

$$\text{and recall } \Omega = \Omega^* (L_{ref}^* / L_{ref}) / a_{ref}^* \text{ (compressible)}$$

$$\text{so with } a_{ref}^* = U_{ref}^* / M_{ref} \text{ and taking } L_{ref}^* = R^*$$

$$\Omega = M_{ref} (U_{tip}^* / U_{ref}^*) / R^* \quad \text{(compressible)}$$

$$\Omega = U_{tip}^* / U_{ref}^* / R^* \quad \text{(incompressible)}$$



# Nondimensional Input (2/2)

- Nondimensional time step:

$$\text{time for one rev: } T^* = 2\pi / \Omega^* = 2\pi R^* / U_{tip}^* \text{ (s)}$$

$$\text{and recall } t = t^* a_{ref}^* (L_{ref} / L_{ref}^*) \text{ (compressible)}$$

so with  $L_{ref}^* = R^*$  we have

$$T = a_{ref}^* (R / R^*) 2\pi R^* / U_{tip}^* = 2\pi R / (M_{ref} U_{tip}^* / U_{ref}^*) \text{ (nondim time / rev)}$$

For N steps per rotor revolution:

$$\Delta t = 2\pi R / (N M_{ref} U_{tip}^* / U_{ref}^*) \text{ (compressible)}$$

$$\Delta t = 2\pi R / (N U_{tip}^* / U_{ref}^*) \text{ (incompressible)}$$

- Note: the azimuthal change per time step is output to the screen in the **Rotor info** section. Make sure this is consistent, to a high degree of precision (say at least 4 digits), with your choice of N steps per rev – you want the blade to end up very close to 360 deg. after multiple revs!
- Formulas above are general, but recall we usually have ref = tip, at least for compressible flow



# CAMRAD Considerations

- User must set up basic CAMRAD II scripts; the `RUN_LOOSE_COUPLING` script provided with FUN3D requires 3 distinct, but related CAMRAD scripts
  - `basename_ref.scr`
    - Used to generate the reference motion data used by CAMRAD
    - Set this file to use rigid blades; zero collective/cyclic; no trim
  - `basename_0.scr`
    - Used for coupling/trim cycle “0”
    - Set up for elastic blades with trim; use CAMRAD aerodynamics exclusively (no delta airloads input); simplest aero model will suffice
  - `basename_n.scr`
    - Used for all subsequent coupling/trim cycles
    - Set up for elastic blades with trim; use same simple CAMRAD aerodynamics but now with delta airloads input



# Untrimmed Rigid-Blade Simulations

- Overview of the basic steps
  1. Prepare rotor blade and fuselage grids, with proper axis orientation
  2. Set up the **rotor.input** file based on desired flight conditions
  3. Run the **dci\_gen** utility to create a composite mesh and initial dci data
  4. Set up **fun3d.nml** and **moving\_body.input** files
  5. Optionally set up the **&slice\_data** namelist in the **fun3d.nml** file
  6. Run the solver with the following command line options (in addition to any other appropriate ones, like **--temporal\_err\_control**)

```
--moving_grid --overset --overset_rotor --dci_on_the_fly  
--dci_period 360 --reuse_existing_dci
```

If optional step 5 is used, add the following (N as desired, typically 1)

```
--slice_freq N --output_comprehensive_loads
```
  7. Number of time steps required is case dependent – usually at least 3 revs

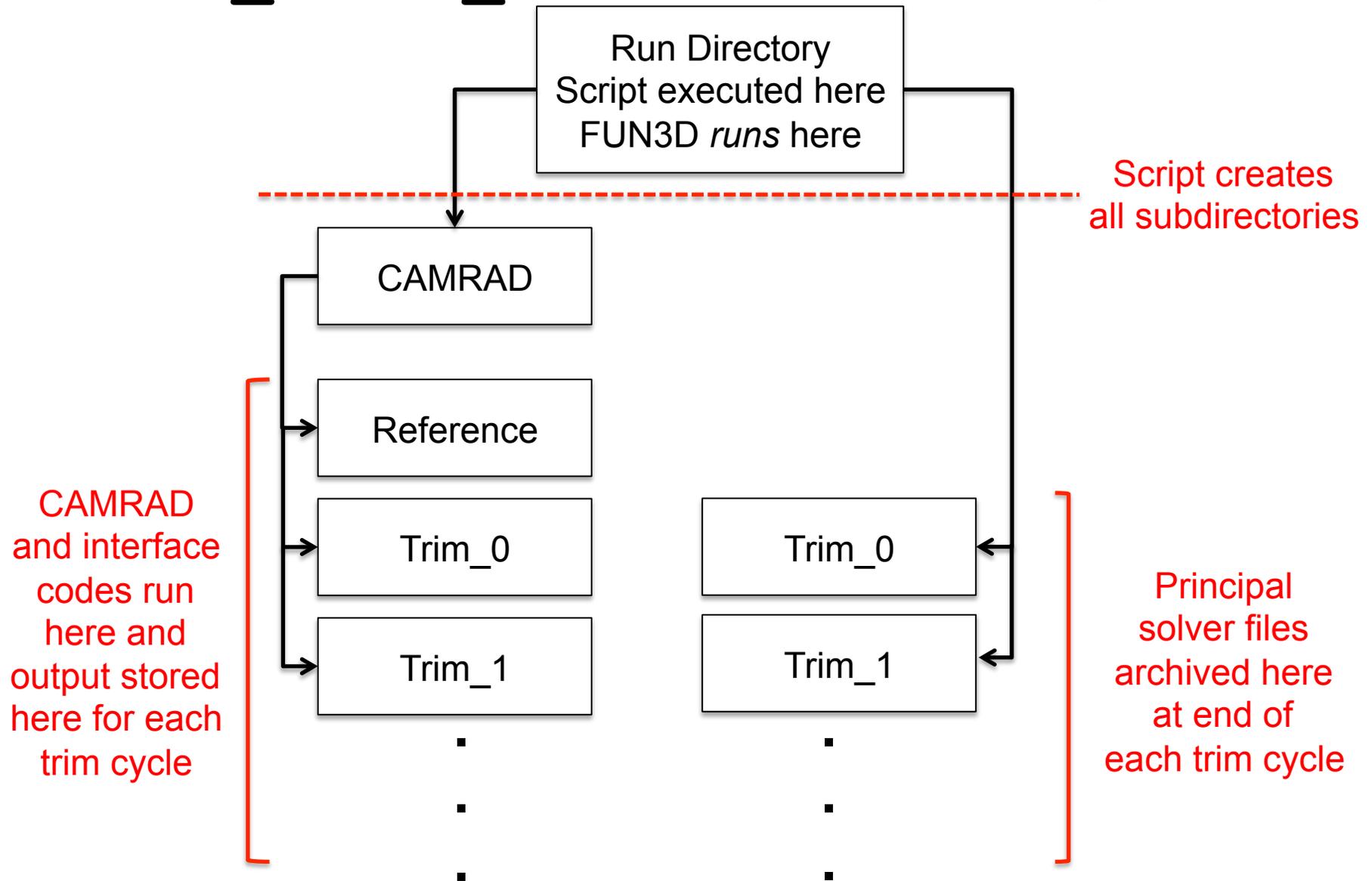


# Trimmed, Elastic-Blade Simulations

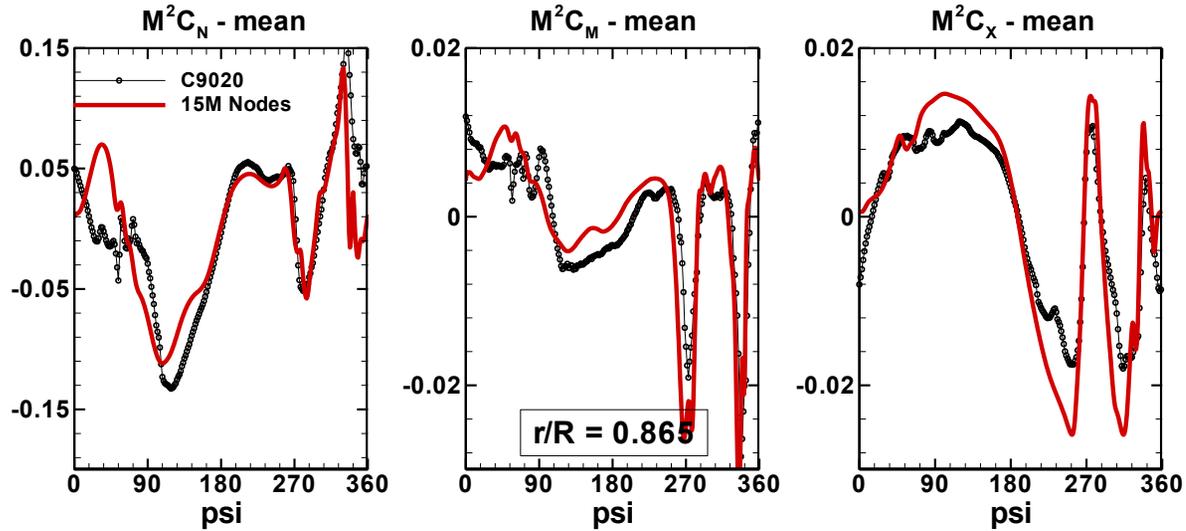
- Overview of the basic steps; steps 1-4 are the same as for the untrimmed rigid-blade case; use of CAMRAD is assumed
  5. Set up the `&slice_data` namelist; *not optional*
  6. Set up the 3 CAMRAD run-script templates
  7. Set up the `RUN_LOOSE_COUPLING` run script (a c-shell script geared to PBS environments); user-set data is near the top – sections 1 and 2
  8. Set up the `fun3d.nml_initial` and `fun3d.nml_restart` files used by the run script; typically set the time steps in the initial file to cover 2 revs, and  $2/N_{\text{blade}}$  revs in restart version
  9. If using the run script make sure all items it needs are in place; script checks for missing items, but it gets old having to keep restarting because you forgot something!
  10. Number of coupling cycles required for trim can vary, but 8-10 is typical for low-moderate thrust levels; high thrust cases near thrust boundary may require 10-15; user judges acceptable convergence



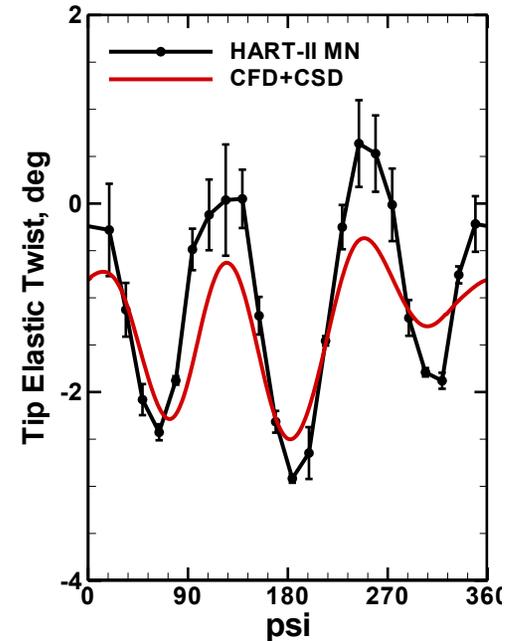
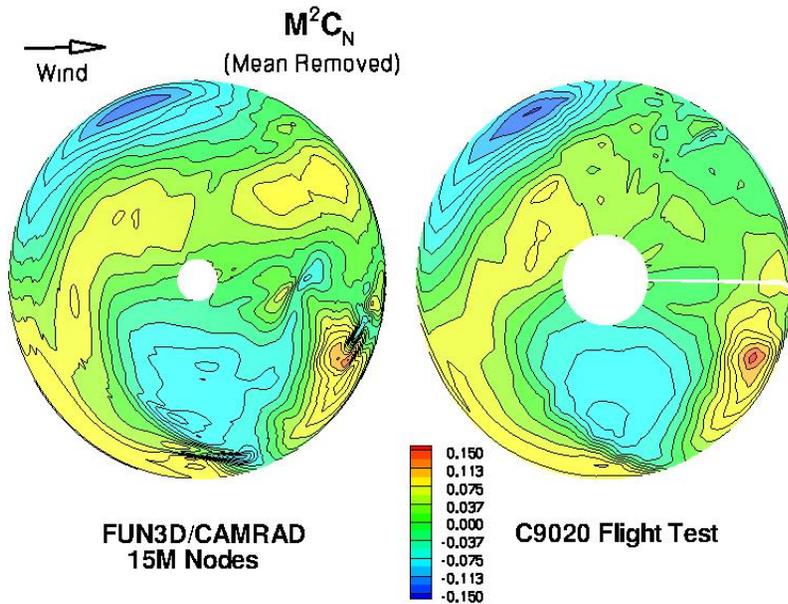
# RUN\_LOOSE\_COUPLING Directory Tree



# Postprocessing



Sample Plots Possible Via  
process\_rotor\_airloads.f90  
Output



# The End

